# BASIN-WIDE EVALUATION OF THE UPPERMOST GREEN RIVER FORMATION'S OIL-SHALE RESOURCE, UINTA BASIN, UTAH AND COLORADO

by Michael D. Vanden Berg



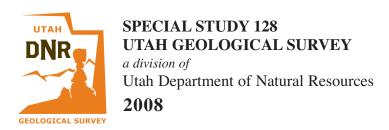


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**Cover photo:** A sample of Utah oil shale collected from the White River Mine.

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# BASIN-WIDE EVALUATION OF THE UPPERMOST GREEN RIVER FORMATION'S OIL-SHALE RESOURCE, UINTA BASIN, UTAH AND COLORADO

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#### **ABSTRACT**

Due to the recent increase in crude oil prices and concerns over diminishing conventional reserves, the Utah Geological Survey has reexamined the Uinta Basin's oil-shale resource, primarily in the Mahogany zone of the Green River Formation. Past assessments, the first conducted in 1964 and subsequent studies continuing through the early 1980s, concentrated on the Eocene Green River Formation's Mahogany zone in the southeastern part of the Uinta Basin, and were limited in the amount of drill hole data available at the time. We have broadened the investigation to include the entire Uinta Basin, taking advantage of the hundreds of geophysical logs from oil and gas wells drilled over the last two decades. We created conversion equations by correlating available Fischer assays with corresponding density and sonic measurements as a way to predict oil yield from geophysical logs. In addition to the core-based Fischer assays obtained from 107 wells drilled specifically for oil shale, 186 oil and gas wells with oil yields calculated from digitized bulk density or sonic logs were used to create a basin-wide picture of the oil-shale resource in the Uinta Basin. These widespread data were used to map oil-shale thickness and richness and create isopach maps delineating oil yields of 15, 25, 35, and 50 gallons of shale oil per ton (GPT) of rock. Thicknesses were centered around the extremely rich Mahogany bed of the Mahogany zone (R-7) within the Parachute Creek Member of the Green River Formation. From these isopach maps, new basin-wide resource numbers were calculated for each richness grade. In addition, oil-shale resource numbers were adjusted according to different sets of constraints, including resources less than 3000 feet deep, resources located on specific landownership categories, and resources associated with conventional oil and gas fields.

The thickest and richest oil-shale zones are located in central Uintah County in T. 8 S. to T. 12 S. and R. 20 E. to R. 25 E., Salt Lake Base Line and Meridian. Overburden in these areas ranges from zero at the outcrop in the east, to almost 4000 feet farther to the northwest. A continuous interval of oil shale averaging 50 GPT contains an in-place oil resource of 31 billion barrels in a zone ranging up to 20 feet thick. Where the 50 GPT interval is at least 5 feet thick and less than 3000 feet deep, the in-place resource drops to 26 billion barrels. An interval averaging 35 GPT, with a maximum thickness of 55 feet, contains an in-place oil resource of 76 billion barrels. Where this interval is at least 5 feet thick and less than 3000 feet deep, the total in-place resource drops to 61 billion barrels. The 25 GPT zone and the 15 GPT zone contain unconstrained resources of 147 billion barrels and

292 billion barrels, respectively. The maximum thickness of 25 GPT rock is about 130 feet, whereas the maximum thickness of 15 GPT rock is about 500 feet. Where these two intervals are at least 5 feet thick and less than 3000 feet deep, the 25 GPT resource drops to 111 billion barrels and the 15 GPT resource drops to 228 billion barrels.

The 25 GPT resource calculated for U.S. Bureau of Land Management (BLM) lands that could be considered for commercial oil-shale leasing is approximately 69 billion barrels, roughly 50% of Utah's total oil-shale resource. The remaining resource is located on tribal (20%), private (16%), state trust (9%), U.S. Forest Service (3%), and protected land (2%) such as state wildlife reserves, national wildlife refuges, state sovereign lands, and state parks. Furthermore, approximately 25% of Utah's oil-shale resource lies within existing oil or gas fields, creating resource conflict issues that will need to be addressed as conventional and unconventional resources are developed.

After placing several constraints on Utah's total in-place oil-shale resource, we determined that approximately 77 billion barrels of oil could be considered as a potential economic resource. This estimate is for deposits that are at least 25 GPT; at least 5 feet thick; under less than 3000 feet of cover; not in conflict with current conventional oil and gas resources; and located only on BLM, state, private, and tribal lands.

## INTRODUCTION AND BACKGROUND

In the 1960s, the U.S. Department of Interior started an aggressive program to describe and estimate the Green River Formation oil-shale resource. The dramatic increase in petroleum prices resulting from the Organization of the Petroleum Exporting Countries (OPEC) oil embargo of 1973 triggered a second resurgence of oil-shale research during the 1970s and early 1980s. When oil prices plummeted in the mid-1980s, so did research associated with oil shale. With recent crude oil prices again rising to new heights, and as conventional crude oil supplies continue to diminish, interest in unconventional fuel sources such as oil shale has been renewed.

The largest known oil-shale deposits in the world are in the Eocene Green River Formation, which covers portions of Utah, Colorado, and Wyoming (figure 1). Lacustrine sediments of the Green River Formation were deposited in two large lakes that occupied a 25,000-square-mile area in the Piceance, Uinta, Green River, and Washakie sedimentary basins. Fluctuations in stream inflow caused large expan-

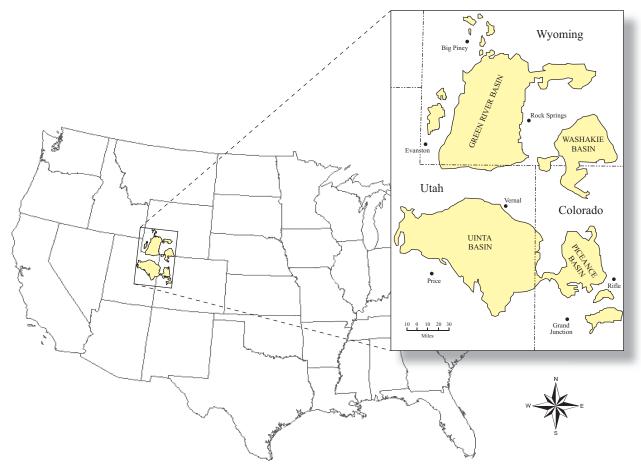


Figure 1. Oil-shale resource areas of Utah, Colorado, and Wyoming (adapted from Bartis and others, 2005, and Bunger and others, 2004).

sions and contractions of the lakes, as evidenced by widespread intertonguing of marly lacustrine strata with beds of land-derived sandstone and siltstone. During arid times, the lakes contracted in size and the lake waters became increasingly saline and alkaline (Dyni, 2003). The warm alkaline waters provided excellent conditions for the abundant growth of cyanobacteria (blue-green algae), which is thought to be the major precursor of the organic matter in the oil shale (Dyni, 2003). The organic matter preserved in the shale is called kerogen, which when heated can produce crude oil and natural gas. Figure 2 shows a stratigraphic section of the Parachute Creek Member of the upper Green River Formation in the Uinta Basin, Utah as it appears in corehole U044 (section 22, T. 9 S., R. 23 E., Salt Lake Base Line and Meridian [SLBLM]). The section with the richest oil shale is named the Mahogany zone (R-7), where individual beds, such as the Mahogany bed, can exceed 70 gallons of oil per ton of rock and the entire zone is commonly over 100 feet thick.

The entire length of the Mahogany zone outcrop has been mapped at the 1:100,000 and/or 1:24,000 scale and defines the southern boundary of the study area. The southeastern extent of the outcrop was digitized from 14 7.5-minute quadrangles, and the remaining sections of outcrop were digitized from three 30' x 60' geologic maps. The 14 7.5-minute quadrangles are Agency Draw NE (Pipiringos, 1979), Agency Draw NW (Cashion, 1984), Bates Knolls (Pipiringos, 1978), Burnt Timber Canyon (Keighin, 1977a), Cooper Canyon (Keighin, 1977b), Davis Canyon (Pantea,

1987), Dragon (Scott and Pantea, 1985), Flat Rock Mesa (Pantea and Scott, 1986), Nutters Hole (Cashion, 1994), Rainbow (Keighin, 1977c), Southam Canyon (Cashion, 1974), Walsh Knolls (Cashion, 1978), Weaver Ridge (Cashion, 1977), and Wolf Point (Scott and Pantea, 1986). The 30' x 60' maps are the Huntington (Witkind, 1988), Price (Weiss and others, 1990), and Westwater (Gualtieri, 1988).

Estimates of the in-place oil-shale resource within the entire Green River Formation range from 1.5 trillion (Smith, 1980; Dyni, 2003) to 1.8 trillion barrels (Culbertson and Pitman, 1973; U.S. Federal Energy Administration, 1974). Historical estimates of the Utah portion of this resource vary from 165 billion barrels (Smith, 1980) to 214 billion barrels (Trudell and others, 1983) to 321 billion barrels (Cashion, 1964). Colorado and Wyoming are thought to contain 1.0 trillion and 300 billion barrels, respectively (Smith, 1980; Pitman and others, 1989; Culbertson and others, 1980; Trudell and others, 1973). These in-place resource estimates are based on oil shale with a minimum grade of 15 gallons per ton with no constraints on overburden thickness, which in Utah can reach over 9000 feet. In addition, these in-place resource numbers should not be compared to conventional oil reserves, as is often the case (a resource is the total amount of a particular commodity available in the ground, a reserve is the amount of that commodity that can be economically recovered). No commercial technology is currently available to extract oil from oil shale; therefore, accurate reserve numbers can not be calculated.

With previous Utah-based studies typically only utiliz-

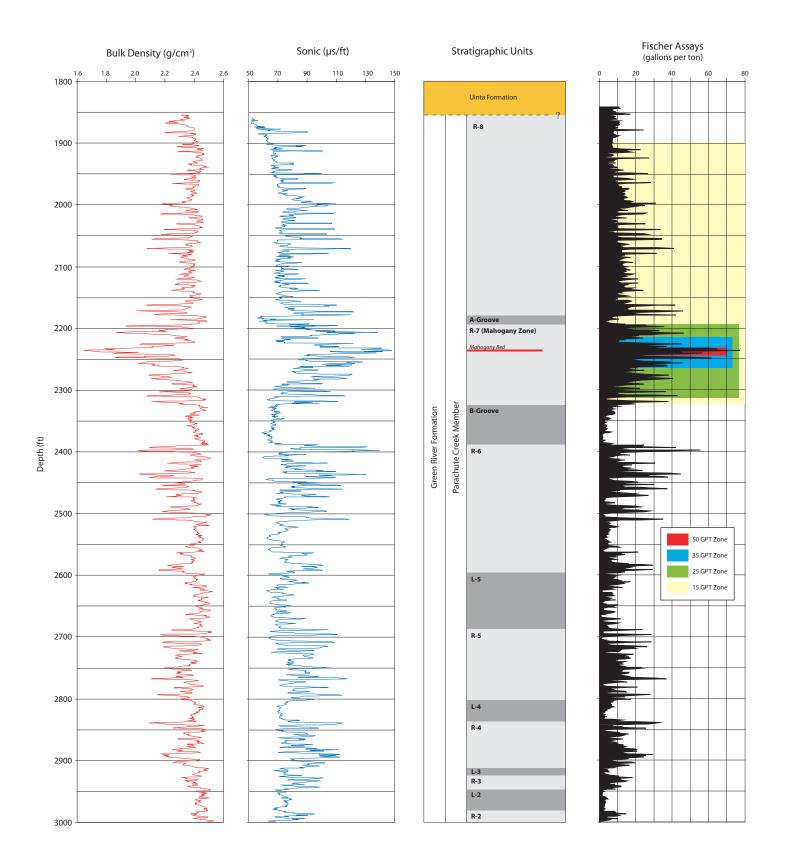


Figure 2. Stratigraphy of the Parachute Creek Member of the upper Green River Formation illustrated by bulk density, sonic, and oil-yield plots from well U044 (section 22, T. 9 S., R. 23 E., SLBLM). "R" refers to a rich oil-shale zone and "L" refers to a lean oil shale zone (stratigraphic nomenclature for oil-shale zones derived from Donnell and Blair, 1970, and Cashion and Donnell, 1972).

ing oil-shale-specific wells drilled in Uintah County, earlier resource estimates had to rely heavily on extensive extrapolation into areas having no drill holes or oil-yield analyses. In addition, each study looked at different oil-shale horizons. For example, Trudell and others (1983) looked at oil shale only within and above the Mahogany zone, while significant resources are also available in the shales below this horizon (figure 2).

Roughly 180 oil-shale-specific wells were drilled between 1954 and 1983 and their cores were analyzed for oil yield using the modified Fischer assay technique, as described by Stanfield and Frost (1949) and later adopted by the American Society for Testing and Materials (1980). This method was developed primarily for evaluating the Green River oil-shale resources. Generally, the assays of drill cores were made on crushed samples prepared from one- or twofoot lengths of quartered core. A complete database of Fischer assays for wells from the state of Utah can be found in Vanden Berg and others (2006). These wells were typically located in central to southern Uintah County, typically near the well-mapped outcrop of the Mahogany zone, the richest oil-shale horizon. A few wells, drilled farther west and north, reached the Mahogany zone at more than 2000 feet below the surface.

Fischer assays were also performed on rotary cuttings from oil and gas wells averaged over 10-foot intervals. However, these data are unreliable due to contamination by mixing of cuttings, contamination from borehole cave-ins, and depth errors resulting when the samples were inaccurately lagged for travel time up the borehole. Also, with averages over such a wide spacing, accurate zone thicknesses could not be calculated, especially for the 50 GPT zone. Because these data are generally unreliable and typically underestimate the resource, assays from rotary cuttings were not used in this study.

#### **METHODS**

#### **Resource Calculations and Isopach Maps**

The first step in creating a basin-wide oil-shale resource assessment was to determine how geophysical logs from hundreds of oil and gas wells in the region could be related to the oil yield of oil shale. Previous researchers determined that bulk density logs display an excellent inverse correlation to oil yield obtained using the modified Fischer assay technique; the more kerogen-rich the oil shale, the less dense the material (Bardsley and Algermissen, 1963; Tixier and Curtis, 1967; Smith and others, 1968; Dyni and others, 1991) (figures 2 and 3, table 1). A sonic log also shows a correlation with oil yield, albeit not as significant as bulk density, displaying higher travel times in the less dense, kerogen-rich intervals (figures 2 and 3, table 1). To characterize these correlations, UGS digitized old paper copies of bulk density and sonic logs from oil-shale wells that also had core-based oil yields determined by Fischer assay. The core-based Fischer assays were typically performed on a one-foot spacing, with half-foot spacing in the highest yielding zones and up to three-foot spacing in the leaner zones. Bulk density logs from 14 wells and sonic logs from nine wells were digitized using Neuralog software. Several other wells having both density or sonic logs and oil-yield data were available; however, many logs lacked identifiable scaling, while other wells contained large data gaps within the oil-yield analyses. After digitizing the logs at half-foot intervals, cross-plots were generated relating the bulk density or sonic measurements with oil yields after they were fitted to the same half-foot depth scale. Next, the cross-plots were analyzed using a simple linear regression model (table 1). In some cases, the log data needed to be manually shifted along the depth scale to match with the corresponding intervals measured for oil yield. This was done by visually comparing the two curves and matching various peaks and zones. In addition, spurious data spikes were eliminated from the Fischer assays and the digital logs.

After analyzing the individual regressions, we discarded wells having poor results, typically R<sup>2</sup> values less than 0.7 for density logs and less than 0.6 for sonic logs. This left a total of eight wells relating bulk density to oil yield, with Mahogany bed depths ranging from 100 to 2650 feet, and four wells relating sonic to oil yield, with Mahogany bed depths ranging from 660 to 2230 feet (table 1).

Since both variables, the geophysical and oil-yield logs, are subject to measurement errors, we decided to apply a reduced-major-axes fit to a combination of all the data. This was done separately for both the bulk density and sonic logs creating an equation for each (figure 3, table 1). This method provided two robust equations that could be applied to other wells with density or sonic logs located throughout the basin and at various depths. The equation for relating bulk density to oil yield in gallons per ton was determined to be:

(1) oil yield = 
$$-80.894\rho + 203.996$$

were  $\rho$  equals the bulk density value in grams per cubic centimeter (g/cm<sup>3</sup>). The equation for relating sonic logs to oil yield in gallons per ton was determined to be:

(2) oil yield = 
$$0.766\Delta\tau - 49.237$$

were  $\Delta\tau$  equals travel time in microseconds per foot (µs/ft). Dyni and others (1991) argued that the regression was slightly improved for the sonic logs with a second-degree polynomial equation. However, this study found that a second-degree polynomial, even though the  $R^2$  was slightly higher, calculated oil yields notably higher than nearby wells with Fischer assay analyses. The simpler linear equation shown above (2) was determined to be more robust.

After the equations relating oil yield to geophysical log were created, oil and gas wells with these particular logs had to be found throughout the Uinta Basin. The goal was to try to find at least one well per township, while adding additional wells in areas of particular interest. One difficulty was finding wells with log data for the oil-shale-bearing portion (i.e., Mahogany zone) of the Green River Formation. Since many oil and gas wells in the basin have targets far below this formation, several companies simply did not log the upper part of the borehole. After an extensive search, 186 wells, 167 with adequate bulk density logs and 19 with adequate sonic logs, were chosen (see appendix). Since density logs display a better correlation with oil yield, preference was given to those logs. Wells with sonic logs were used to fill in data gaps. Unfortunately, only image files of these logs exist, at least in the public domain, so all logs had to be manually digitized using NeuraLog software.

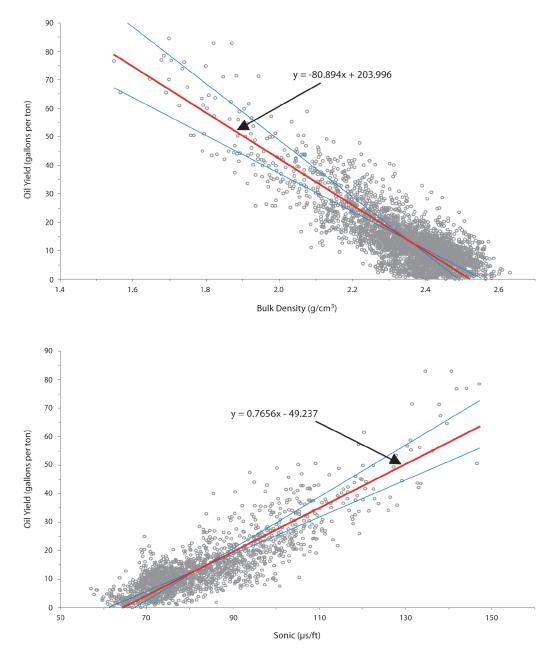


Figure 3. Reduced-major-axes regression relating bulk density and sonic log readings to oil yield.

With the creation of digitized geophysical logs in which data were recorded on a half-foot spacing, the above equations could be systematically applied to create calculated oilyield logs for all 186 wells. In cases of particularly high density or particularly low sonic values, the equations predicted negative yield values. These negative intervals were adjusted to equal zero gallons per ton.

The next step was to calculate the thickness of continuous intervals of oil shale averaging 15, 25, 35, and 50 gallons per ton. These intervals were determined for all 186 oil and gas wells with calculated assay data, as well as 107 oil-shale-specific wells with assays derived from core, for a total of 293 wells. These continuous zones were calculated starting at the Mahogany bed, adding assay values above or below until the desired average oil yield was found (see appendix). In some cases, the depth interval measured by the log or Fischer assay was limited, and a total thickness for the 15 and/or

25 GPT zone could not be found. When this occurred, the thickness was estimated using a ratio of the thicknesses of the 25/15 GPT zones, or the 35/25 GPT zones, from a nearby well. These estimated values are indicated by italic font in the appendix.

Using ArcGIS software, isopachs for the thickness of each richness zone were plotted using a spline fit with tension. In some cases, individual thickness values were edited to remove spurious "bulls-eyes" from the isopachs; these edited values are indicated in italic font in the appendix. The northern boundary of the isopachs is simply the extent of the available data, whereas the southern boundary is delineated by the outcrop of the Mahogany zone. The area mapped was divided into the smallest thickness intervals possible—0.1 feet for the 50 GPT zone, 0.25 feet for the 35 GPT zone, 0.5 feet for the 25 GPT zone, and 2.5 feet for the 15 GPT zone—and the sub-areas underlain by each thickness interval were

USGS#	Bul	k Density I	og	S	onic Log	
	Individual		RMA equation	Individual		RMA equation
	regression equation	$\mathbb{R}^2$	relating all data	regression equation	$\mathbb{R}^2$	relating all data
U153	y=-90.69x + 223.95	0.76				
U061				y=0.76x - 48.33	0.69	
U065	y=-67.24x + 177.41	0.73		y=0.73x - 45.50	0.69	
U059	y=-66.83x + 173.24	0.71				
U092	y=-75.72x+193.14	0.73	y=-80.894x + 203.996			y=0.766x - 49.237
U085	y=-70.72x+183.35	0.74		y=0.61x - 34.97	0.64	
U044	y=-85.50x + 213.46	0.84		y=0.63x - 38.29	0.77	
U102	y=-68.92x + 178.22	0.73				

**Table 1.** Equations used to calculate oil shale richness from density and sonic logs.

USGS#	Mahogany Bed	Twn	Rng	Sec	Mrd	UTM E	UTM N
	Depth to						
	bed (ft)						
U153	100	12S	24E	25	SL	656186	4401431
U061	659	10S	24E	14	SL	655055	4424178
U065	696	10S	25E	19	SL	657974	4422591
U059	719	10S	25E	19	SL	659426	4421812
U092	1027	9S	25E	16	SL	661008	4432488
U085	1965	9S	24E	32	SL	649994	4427496
U044	2236	9S	23E	22	SL	644158	4431449
U102	2313	9S	21E	26	SL	627029	4429992
U045	2646	9S	22E	1	SL	637424	4436007

0.87

RMA = Reduced Major Axes, Twn = Township, Rng = Range, Sec = Section, Mrd = Meridian, SL = Salt Lake Base Line and Meridian

v = -87.17x + 209.63

calculated using the ArcGIS program. To estimate the oilshale resource, rock volumes were calculated by multiplying the area of a given polygon by its average thickness. The thinner the thickness interval mapped, the more precise the estimated volume and the more precise the resource calculation because a more accurate thickness is applied to each area. Next, the average density (see figure 3) of the given richness was used to calculate the weight of oil shale in tons, which then could be converted to a resource estimate in barrels of in-place oil by multiplying the tons by the assayed or estimated oil yield (in GPT). All calculated resource numbers for each richness zone, separated into various thickness bins, can be found in table 2a. Maps displaying the isopach data, separated into corresponding thickness intervals, are displayed in plates 1, 2, 3, and 4.

U045

#### **Overburden Thickness**

Plates 1, 2, 3, and 4 also display overburden contours indicating the depth to the top of the individual richness zones. These contours were created by subtracting the footage below the surface to the top of the richness interval from the surface elevation of the well to arrive at the elevation of the oil-shale horizon of interest. A structure contour map was generated in ArcGIS displaying the surface of each richness interval in feet above sea level. This structure contour map was then subtracted from a digital elevation model of the Uinta Basin providing accurate overburden thickness contours. A few estimated data points were added in areas having little or no oil-shale data as a means to provide more geologically accurate overburden contours, particularly near the outcrop. Overburden thickness equals zero at the outcrop in the southern and eastern portions of the basin and gradually increases in thickness, up to 9000 feet, to the north.

#### **Economic Constraints**

After total in-place resource estimates were calculated,

several constraints were imposed on the total endowment to offer a more realistic impression of the potentially economic oil-shale resource. We assumed that mining, underground and/or surface mining, would generally not occur where the resource is less than 5 feet thick for 25, 35, and 50 GPT rock or less than 15 feet thick for 15 GPT rock. Also, we assumed that mining would not occur where overburden is more than 3000 feet. In addition, since all land will likely not be available for oil-shale extraction, resource numbers were calculated by landownership. Finally, we assumed that conventional oil and gas and oil-shale deposits will not be simultaneously produced, so oil-shale resources for lands outside and within current conventional oil and gas fields were also calculated. These constrained resource estimates are available in tables 2, 3, and 4 and are described in more detail below.

Constraints based on in-situ processing were not considered since a proven in-situ technique has not been developed. Shell's In-situ Conversion Process (ICP), currently being tested in western Colorado's Piceance Basin, is targeting oil shale from a zone between 1000 to 2000 feet thick that averages roughly 30 to 35 GPT (Shell Oil Company, 2008). Utah's 35 GPT zone reaches only 55 feet in thickness, dramatically thinner than oil-shale resources in Colorado. Other types of in-situ processes might be more adaptable to Utah's thinner deposits in the future, but currently, all in-situ demonstration projects are in the thick deposits of Colorado's Piceance Basin.

#### RESULTS

#### **Total In-Place Resource**

A continuous section of oil shale averaging 50 GPT in the Uinta Basin of Utah contains approximately 31 billion barrels of in-place oil, including approximately 23 billion barrels in deposits between 5 and 20 feet thick (table 2a).

The 50 GPT interval is contained entirely within the Mahogany zone and is centered on the Mahogany bed (R-7, see figure 2). The thickest deposits, 15 to 20 feet, of 50 GPT rock are located in T. 10 S., R. 22-24 E., SLBLM, as well as the northern sections of T. 11 S., R. 24-25 E. and the eastern sections of T. 9 S., R. 21 E. (plate 1). The top of the 50 GPT zone in these areas ranges in depth from 450 to 2500 feet. Potentially economic thicknesses, at least 5 to 10 feet, of 50 GPT rock are near the outcrop on the eastern side of the study area. In addition to the large resource in the eastern part of the basin, a long finger of rich oil shale ranging in thickness from 5 to 10 feet extends westward through the southern portion of Duchesne County. These deposits range from 2000 to 3000 feet below the surface. Oil-shale deposits averaging 50 GPT and located less than 3000 feet below the surface contain approximately 26 billion barrels of oil, including 20 billion barrels found in deposits between 5 and 20 feet thick (table 2b).

A continuous section of oil shale averaging 35 GPT contains approximately 76 billion barrels of in-place oil, including 73 billion barrels in deposits ranging between 5 and 55 feet thick (table 2a). The 35 GPT interval is also contained entirely within the Mahogany zone, centered on the Mahogany bed. The thickest interval, 40 to 55 feet, is located in T. 9 S., R. 21-23 E., SLBLM, and T. 10 S., R. 21-24 E.

(plate 2). The top of the 35 GPT zone in this area ranges in depth from 800 to 2500 feet. Again, reasonably thick deposits, 10 to 40 feet, are located near outcrop along the eastern extent of the study area. Similar to the 50 GPT zone, the 35 GPT zone exhibits a long finger extending westward through the southern part of Duchesne County. This zone reaches 38 feet thick and is located under depths ranging from outcrop to 2500 feet. Oil-shale deposits averaging 35 GPT and located less than 3000 feet below the surface contain approximately 61 billion barrels of oil, including 59 billion barrels found in deposits between 5 and 55 feet thick (table 2b).

A continuous section of oil shale averaging 25 GPT contains approximately 147 billion barrels of in-place oil, including 146 billion barrels in deposits 5 to 130 feet thick (table 2a). The 25 GPT interval is typically within the Mahogany zone; however, in some cases the 25 GPT zone includes part of the A- or B-grooves (figure 2). The thickest interval, 100 to 130 feet, of 25 GPT rock is located in T. 9 S., R. 21-24 E., SLBLM, T. 10 S., R. 22-24 E., and other small areas within T. 8 S., R. 20-23 E. (plate 3). The top of these deposits ranges in depth from 750 to roughly 3500 feet. Near the outcrop, on the eastern side of the basin, deposits averaging 25 GPT are 40 to 100 feet thick. In southern Duchesne County, the 25 GPT zone ranges up to 60 feet thick with

Table 2a. The Uinta Basin's total Green River Formation oil-shale resource, grouped by grade and thickness.

Thickness (ft)	0-5	5-10	10-15	15-20	•					
Total volume (billion ft <sup>3</sup> )	112.8	198.6	90.8	29.1						
Average density		1.90 g/cm3	(0.0593 tons/fi	t <sup>3</sup> )						
Billion tons	6.7	11.8	5.4	1.7						
Billion barrels	8.0	14.1	6.4	2.1						
Total resource (billion barrels)		3	30.5							
35 GPT										
Thickness (ft)	0-5	5-10	10-20	20-30	30-40	40-55				
Total volume (billion ft <sup>3</sup> )	58.6	155.9	447.8	326.4	269.7	142.6				
Average density			2.09 g/cm <sup>3</sup> (	0.0652 tons/ft	3)					
Billion tons	3.8	10.2	29.2	21.3	17.6	9.3				
Billion barrels	3.2	8.5	24.3	17.7	14.7	7.7				
TC + 1 (1999 1 1)			7	6.1		14.7 7.7				
Total resource (billion barrels)			,	0.1			•			
25 GPT Thickness (ft)	0-5	5-20	20-40	40-60	60-80	80-100	100-130			
25 GPT	0-5 37.6	5-20 366.6			60-80 454.6	80-100 569.7	100-130 448.0			
25 GPT Thickness (ft)			20-40	40-60 765.0	454.6					
25 GPT Thickness (ft) Total volume (billion ft³)			20-40 944.1	40-60 765.0	454.6					
25 GPT Thickness (ft) Total volume (billion ft³) Average density	37.6	366.6	20-40 944.1 2.21 g	40-60 765.0 /cm³ (0.0690	454.6 tons/ft <sup>3</sup> )	569.7	448.0			
25 GPT Thickness (ft) Total volume (billion ft³) Average density Billion tons	37.6 2.6	366.6 25.3	20-40 944.1 2.21 g 65.2	40-60 765.0 /cm³ (0.0690 52.8	454.6 tons/ft <sup>3</sup> ) 31.4	569.7 39.3	448.0 30.9			
25 GPT Thickness (ft) Total volume (billion ft³) Average density Billion tons Billion barrels Total resource (billion barrels)	37.6 2.6	366.6 25.3	20-40 944.1 2.21 g 65.2	40-60 765.0 /cm³ (0.0690 52.8 31.5	454.6 tons/ft <sup>3</sup> ) 31.4	569.7 39.3	448.0 30.9			
25 GPT Thickness (ft) Total volume (billion ft³) Average density Billion tons Billion barrels Total resource (billion barrels)	37.6 2.6	366.6 25.3	20-40 944.1 2.21 g 65.2	40-60 765.0 /cm³ (0.0690 52.8 31.5	454.6 tons/ft <sup>3</sup> ) 31.4	569.7 39.3	448.0 30.9			
25 GPT Thickness (ft) Total volume (billion ft³) Average density Billion tons Billion barrels Total resource (billion barrels)  15 GPT Thickness (ft)	37.6 2.6 1.5	366.6 25.3 15.1	20-40 944.1 2.21 g 65.2 38.8	40-60 765.0 /cm³ (0.0690 52.8 31.5 147.4	454.6 tons/ft³) 31.4 18.7	569.7 39.3 23.4	448.0 30.9			
25 GPT Thickness (ft) Total volume (billion ft³) Average density Billion tons Billion barrels Total resource (billion barrels)  15 GPT Thickness (ft) Total volume (billion ft³)	37.6 2.6 1.5	366.6 25.3 15.1	20-40 944.1 2.21 g 65.2 38.8	40-60 765.0 765.0 (cm³ (0.0690 52.8 31.5 147.4	454.6 tons/ft³) 31.4 18.7 300-400 2650.3	569.7 39.3 23.4	448.0 30.9			
25 GPT Thickness (ft) Total volume (billion ft³) Average density Billion tons Billion barrels Total resource (billion barrels)  15 GPT Thickness (ft) Total volume (billion ft³) Average density	37.6 2.6 1.5	366.6 25.3 15.1	20-40 944.1 2.21 g 65.2 38.8	40-60 765.0 765.0 52.8 31.5 147.4	454.6 tons/ft³) 31.4 18.7 300-400 2650.3	569.7 39.3 23.4	448.0 30.9			
25 GPT Thickness (ft) Total volume (billion ft³) Average density Billion tons Billion barrels	37.6 2.6 1.5	366.6 25.3 15.1 15-100 3178.8	20-40 944.1 2.21 g 65.2 38.8 100-200 2776.4 2.34 g/cm <sup>3</sup> (	40-60 765.0 /cm³ (0.0690 52.8 31.5 147.4 200-300 1568.2 0.0730 tons/ft²	454.6 tons/ft³) 31.4 18.7 300-400 2650.3	569.7 39.3 23.4 400-500 916.7	448.0 30.9			

Note: Totals may not equal sum of components because of independent rounding

GPT = gallons of shale oil per ton of rock (42 gallons/barrel)

**Table 2b.** The Uinta Basin's total Green River Formation oil-shale resource with less than 3000 feet of overburden, grouped by grade and thickness.

50 GPT							
Thickness (ft)	0-5	5-10	10-15	15-20			
Total volume (billion ft <sup>3</sup> )	82.1	172.1	80.1	29.1			
Average density		1.90 g/cm <sup>3</sup> (	0.0593 tons/ft	3)			
Billion tons	4.9	10.2	4.8	1.7			
Billion barrels	5.8	12.2	5.7	2.1			
Total resource (billion barrels)		25	5.7				
35 GPT							
Thickness (ft)	0-5	5-10	10-20	20-30	30-40	40-55	-
Total volume (billion ft <sup>3</sup> )	32.1	75.0	366.4	280.9	228.4	141.5	
Average density			2.09 g/cm <sup>3</sup> (	0.0652 tons/ft	3)		
Billion tons	2.1	4.9	23.9	18.3	14.9	9.2	
Billion barrels	1.7	4.1	19.9	15.3	12.4	7.7	
Total resource (billion barrels)			61	1.1			
25 GPT							
Thickness (ft)	0-5	5-20	20-40	40-60	60-80	80-100	100-130
Total volume (billion ft <sup>3</sup> )	28.7	192.0	659.5	601.4	363.0	480.5	414.0
Average density			2.21 g/	cm <sup>3</sup> (0.0690	tons/ft³)		
Billion tons	2.0	13.3	45.6	41.5	25.1	33.2	28.6
Billion barrels	1.2	7.9	27.1	24.7	14.9	19.8	17.0
Difficial daries				112.6			

Note: Totals may not equal sum of components because of independent rounding

0-15

105.0

7.7

2.7

15-100

1890.7

137.9

49 2

100-200

1986.1

144.8

517

2.34 g/cm<sup>3</sup>

200-300

1227.1

 $(0.0730 \text{ tons/ft}^3)$ 

89.5

32.0

228.3

300-400

2640.0

192.5

68.8

GPT = gallons of shale oil per ton of rock (42 gallons/barrel)

deposits roughly 500 to 3000 feet deep. Deposits averaging 25 GPT that are located less than 3000 feet below the surface contain approximately 113 billion barrels of oil, including 111 billion barrels found in deposits between 5 and 130 feet thick (table 2b).

Thickness (ft)

Average density

Billion tons

Billion barrels

Total volume (billion ft3)

Total resource (billion barrels)

Finally, a continuous section of oil shale averaging 15 GPT contains approximately 292 billion barrels of in-place oil, including 289 billion barrels available in deposits greater than 15 feet thick (table 2a). This resource estimate is 10% lower than Cashion's 1964 in-place oil-shale resource estimate of 321 billion barrels for deposits containing at least 15 GPT at a minimum thickness of 15 feet. The availability of more drill hole data allows the new estimate to be more reliable than Cashion's (1964) estimate by identifying the areas of thick, rich oil shale more precisely. The 15 GPT interval includes all or parts of the R-6, B-Groove, R-7 (Mahogany Zone), A-Groove, and R-8 oil-shale zones (see figure 2). The thickest intervals, 400 to 500 feet, are primarily located in T. 9 S., R. 21-25 E., SLBLM, and T. 10 S., R. 23-24 E. where depths to the top of the zone range between 600 and 2300 feet (plate 4). Deposits near the eastern outcrop range from 100 to 400 feet thick. Deposits averaging 15 GPT that are less than 3000 feet below the surface contain approximately 228 billion barrels of oil, including 226 billion barrels in deposits between 15 and 500 feet thick (table 2b).

400-500

916.7

66.9

23 9

#### **Resource by Landownership**

Table 3 shows a breakdown of the Uinta Basin's oil-shale resource by landownership. Roughly 50% of oil shale is located on lands administered by the BLM. Tribal, private, state trust, and U.S. Forest Service lands hold the next-largest resource with about 20%, 16%, 9%, and 3% of total, respectively (average for all grades). The remaining 2% is locked up in protected lands such as state wildlife reserves, national wildlife refuges, state sovereign lands (mostly land under the Green River), and state parks. In addition, less than 1% of the Uinta Basin's oil-shale resource lies over the border in Colorado.

Plate 5 shows 25 GPT isopach contours displayed over top of landownership. The thickest interval of 25 GPT rock, between 100 and 130 feet thick, is located primarily on BLM land and contains 13.5 billion barrels or 73% of the resource at this thickness and richness. Several state blocks and large areas of private land are located near the eastern outcrop of

Table 3. The Uinta Basin's total Green River Formation oil-shale resource grouped by grade, thickness, and landownership.

50 GPT	(resource	numbers in	billion	barrels)

Thickness (feet)	0-5	5-10	10-15	15-20	Total	% of Total
U.S. Bureau of Land Management	2.7	7.1	4.1	1.6	15.4	50.5%
Indian Reservation	1.8	3.1	0.9	0.2	6.0	19.7%
Private	1.8	1.7	0.6	0.1	4.2	13.8%
State Trust Lands	0.5	1.2	0.8	0.2	2.7	8.9%
U.S. Forest Service	0.9	0.5	0.0	0.0	1.4	4.6%
State Wildlife Reserve - Management area	0.2	0.3	0.0	0.0	0.5	1.6%
U.S. Fish & Wildlife - National Wildlife Refuge	*	*	*	0.0	0.1	0.3%
State Soveriegn Lands	*	*	*	0.0	0.1	0.3%
State Parks and Recreation	*	0.0	0.0	0.0	*	
Colorado Portion	0.1	*	0.0	0.0	0.1	0.3%
Total resource	8.0	14.0	6.4	2.1	30.5	

35 GPT (resource numbers in billion barrels)

Thickness (feet)	0-5	5-10	10-20	20-30	30-40	40-55	Total	% of Total
U.S. Bureau of Land Management	0.9	1.8	9.9	11.4	8.5	5.3	37.7	49.5%
Indian Reservation	0.7	2.0	5.7	2.3	3.0	0.9	14.7	19.3%
Private	1.1	3.4	3.5	1.7	1.8	0.1	11.6	15.2%
State Trust Lands	0.2	0.2	1.7	1.7	1.3	1.4	6.6	8.7%
U.S. Forest Service	0.2	0.7	2.4	0.0	0.0	0.0	3.3	4.3%
State Wildlife Reserve - Management area	0.1	0.2	0.8	0.2	0.0	0.0	1.3	1.7%
U.S. Fish & Wildlife - National Wildlife Refuge	*	*	*	*	0.1	0.0	0.2	0.3%
State Soveriegn Lands	*	*	*	0.1	0.1	0.0	0.2	0.3%
State Parks and Recreation	*	*	0.0	0.0	0.0	0.0	0.1	0.1%
Colorado Portion	0.0	*	0.2	0.3	0.0	0.0	0.5	0.7%
Total resource	3.2	8.5	24.3	17.7	14.7	7.7	76.1	

Thickness (feet)	0-5	5-20	20-40	40-60	60-80	80-100	100-130	Total	% of Total
U.S. Bureau of Land Management	0.5	3.8	13.5	19.0	10.6	10.6	13.5	71.6	48.6%
Indian Reservation	0.4	3.2	8.8	4.4	2.8	6.6	2.1	28.3	19.2%
Private	0.4	5.4	9.7	4.0	2.3	2.9	0.6	25.3	17.2%
State Trust Lands	0.2	0.5	2.0	3.0	1.9	3.1	2.0	12.6	8.5%
U.S. Forest Service	0.1	1.5	3.5	0.0	0.0	0.0	0.0	5.0	3.4%
State Wildlife Reserve - Management area	*	0.5	1.1	0.7	0.0	0.0	0.0	2.3	1.6%
U.S. Fish & Wildlife - National Wildlife Refuge	*	*	0.1	0.1	*	0.1	0.2	0.5	0.3%
State Soveriegn Lands	*	*	*	0.1	0.1	0.1	*	0.3	0.2%
State Parks and Recreation	*	0.2	0.1	0.0	0.0	0.0	0.0	0.3	0.2%
Colorado Portion	0.0	0.0	*	0.2	1.0	0.0	0.0	1.3	0.9%
Total resource	1.5	15.1	38.8	31.5	18.7	23.4	18.4	147.4	

15 GPT (resource numbers in billion barrels)

Thickness (feet)	0-15	15-100	100-200	200-300	300-400	400-500	Total	% of Total
U.S. Bureau of Land Management	1.0	26.0	40.8	22.0	39.9	18.5	148.0	50.6%
Indian Reservation	1.2	17.8	11.3	9.3	12.0	1.0	52.6	18.0%
Private	0.6	25.9	12.0	3.5	6.9	0.6	49.5	16.9%
State Trust Lands	0.4	3.9	6.3	3.3	8.9	3.8	26.6	9.1%
U.S. Forest Service	0.2	6.2	0.0	0.0	0.0	0.0	6.4	2.2%
State Wildlife Reserve - Management area	*	2.3	1.3	0.0	0.0	0.0	3.7	1.3%
U.S. Fish & Wildlife - National Wildlife Refuge	*	0.2	0.2	0.5	0.0	0.0	0.9	0.3%
State Soveriegn Lands	*	*	0.3	0.2	0.0	0.0	0.5	0.2%
State Parks and Recreation	0.0	0.5	0.0	0.0	0.0	0.0	0.5	0.2%
Colorado Portion	0.0	0.0	0.1	2.1	1.4	0.0	3.6	1.2%
Total resource	3.4	82.8	72.3	40.8	69.0	23.9	292.3	

Note: Totals may not equal sum of components because of independent rounding

GPT = gallons of shale oil per ton of rock (42 gallons/barrel)

<sup>\*</sup>Amounts less than 50 million barrels

the Mahogany zone and contain a resource that averages between 40 and 100 feet thick at 25 GPT.

### Resource Conflict with Conventional Oil and Gas Fields

A significant portion of the Uinta Basin's oil-shale resource, approximately 25% for each grade, is covered by conventional oil and gas fields (table 4a and 4b). Plate 6 shows all current oil and gas fields superimposed on the 25 GPT oil-shale isopach. In particular, the extensive Natural Buttes gas field covers a significant portion of land underlain by oil shale averaging 25 GPT, ranging to 130 feet thick, and under roughly 1500 to 4000 feet of cover. Furthermore, this field is expected to expand in size and cover more oil-shale-rich lands to the east. Of the 18.4 billion barrels contained in 25 GPT rock having thicknesses between 100 and 130 feet, 7.8 billion barrels, or 42%, are located under existing natural gas fields (table 4a).

However, lands where the oil-shale deposits are under less than 1000 feet of cover currently do not contain significant oil and gas activity (except the Oil Springs gas field) as compared to lands with deeper oil-shale resources (plate 6). The majority of planned oil-shale operations will be located on lands having less than 1000 feet of cover. This does not mean that oil-shale deposits located within oil and gas fields will be permanently off limits. In fact, most of the conventional oil and gas reservoirs are located far below the Mahogany zone. It simply demonstrates that regulators will need to recognize that resource conflicts exist and plan their lease stipulations accordingly.

# Resource on BLM Lands Proposed for Commercial Leasing

The BLM recently published the Final Programmatic Environmental Impact Statement (PEIS), which finalizes the plan that will guide the use of lands containing oil-shale resources (U.S. Bureau of Land Management, 2008). This is the first step towards a commercial oil-shale leasing program. Within the PEIS, the BLM identified 630,971 acres of public land in Utah's Uintah and eastern Duchesne Counties as having commercial oil-shale development potential (plate 7). These lands are bounded on the north by the 3000-foot overburden contour and bounded on the south by the outcrop of the Mahogany zone. Lands excluded from future leasing include but are not limited to Wilderness Areas, Wilderness Study Areas, river corridors, and lands potentially eligible for Wild and Scenic River status.

We determined that the oil-shale resource on BLM lands proposed for commercial leasing in Utah equals approximately 69 billion barrels at the 25 GPT richness level (table 5). Nearly the entire resource at 25 GPT is between 20 and 130 feet thick. This resource includes roughly 11 billion barrels contained in deposits on the Hill Creek Extension of the Uintah and Ouray Tribal Lands, of which the surface rights are owned by the Ute Indian Tribe.

#### **Potential Economic Resource**

To calculate a more realistic resource estimate for oil-shale deposits located in the Uinta Basin of Utah and Colorado, the UGS applied several constraints to the overall total in-place resource numbers. These constraints are subjective since commercial oil-shale technologies on which to base them do not exist. The constraints used were:

- 1) deposits having a richness of at least 25 GPT,
- 2) deposits that are at least 5 feet thick,
- 3) deposits under less than 3000 feet of cover,
- 4) deposits that are not in direct conflict with current conventional oil and gas operations, and
- 5) deposits located only on BLM, state trust, private, and tribal lands.

With the above-mentioned constraints, the Uinta Basin's potential economic oil-shale resource equals approximately 77 billion barrels (table 6). Plate 8 shows the area within the basin of these constrained resources. This is roughly 26% of the total unconstrained resource calculated at 15 GPT of 292 billion barrels and 52% of the total unconstrained resource calculated at 25 GPT of 147 billion barrels, and is a more realistic estimate of potential recoverable resource. However, this number should not be used as an estimate of recoverable reserves, which cannot be calculated until a proven commercial technology is developed.

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Table 4a. The amount of Uinta Basin oil-shale resource within existing conventional oil and gas fields.

50 GPT (resource numbers in billion barrels) Thickness (feet) 0-5 5-10 10-15 15-20 Total % of Total Located within a current oil or gas field 1.3 3.2 2.2 0.8 7.5 24.6% 4.2 Located outside a current oil or gas field 6.7 10.9 1.2 23.0 75.4% Total resource 8.0 14.0 6.4 2.1 30.5 35 GPT (resource numbers in billion barrels) 0-5 5-10 40-55 Thickness (feet) 10-20 20-30 30-40 Total % of Total Located within a current oil or gas field 0.8 2.2 5.0 3.3 4.4 4.3 19.8 26.0% Located outside a current oil or gas field 2.4 6.3 19.4 14.4 10.3 3.5 56.3 74.0%Total resource 3.2 8.5 24.3 17.7 14.7 7.7 76.1 25 GPT (resource numbers in billion barrels) Thickness (feet) 0-5 5-20 20-40 40-60 60-80 80-100 100-130 Total % of Total Located within a current oil or gas field 0.1 4.1 10.9 5.2 3.9 8.2 7.8 40.3 27.3% Located outside a current oil or gas field 1.4 11.0 27.9 26.2 14.8 15.2 10.6 107.1 72.7% 1.5 31.5 147.4 Total resource 15.1 38.8 18.7 23.4 18.4 15 GPT (resource numbers in billion barrels) Thickness (feet) 0-15 15-100 100-200 200-300 300-400 400-500 Total % of Total Located within a current oil or gas field 0.2 25.0 12.7 26.4 83.3 28.5% 11.9 6.9 209<u>.0</u> 3.2 57.8 59.6 28.9 17.0 71.5% Located outside a current oil or gas field 42.6 **Total resource** 3.4 82.8 72.3 40.8 69.0 23.9 292.3

Note: Totals may not equal sum of components because of independent rounding

GPT = gallons of shale oil per ton of rock (42 gallons/barrel)

Table 4b. The amount of Uinta Basin oil-shale resource within existing conventional oil and gas fields and located under less than 3000 feet of cover.

50 GPT (resource numbers in billion barrels)									
Thickness (feet)	0-5	5-10	10-15	15-20	Total	% of Total			
Located within a current oil or gas field	0.7	2.7	2.2	0.8	6.4	24.9%			
Located outside a current oil or gas field	5.1	9.5	3.5	1.2	19.3	75.1%			
Total resource	5.8	12.2	5.7	2.1	25.7				
35 GPT (resource numbers in billion barrels)									_
Thickness (feet)	0-5	5-10	10-20	20-30	30-40	40-55	Total	% of Total	_
Located within a current oil or gas field	0.1	0.5	3.9	2.8	3.9	4.3	15.5	25.4%	
Located outside a current oil or gas field	1.7	3.6	16.0	12.4	8.5	3.4	45.6	74.6%	_
Total resource	1.7	4.1	19.9	15.3	12.4	7.7	61.1		_
25 GPT (resource numbers in billion barrels)									
Thickness (feet)	0-5	5-20	20-40	40-60	60-80	80-100	100-130	Total	% of Total
Located within a current oil or gas field	*	0.7	4.8	4.7	3.2	7.4	7.1	28.0	24.9%
Located outside a current oil or gas field	1.1	7.2	22.3	20.0	11.7	12.3	9.9	84.6	75.1%
Total resource	1.2	7.9	27.1	24.7	14.9	19.8	17.0	112.6	
15 GPT (resource numbers in billion barrels)									_
Thickness (feet)	0-15	15-100	100-200	200-300	300-400	400-500	Total	% of Total	_
Located within a current oil or gas field	0.1	7.2	9.9	9.3	26.2	6.9	59.7	26.1%	
Located outside a current oil or gas field	2.6	42.0	41.8	22.6	42.5	17.0	168.6	73.9%	_
Total resource	2.7	49.2	51.7	32.0	68.8	23.9	228.3		

Note: Totals may not equal sum of components because of independent rounding

GPT = gallons of shale oil per ton of rock (42 gallons/barrel)

<sup>\*</sup>Amounts less than 50 million barrels

<b>Table 5.</b> The amount of Utah's 25-GPT oil-shale resource
found on lands proposed by the BLM as having commercial
oil-shale leasing potential.

		Resource within the Hill Creek
Thickness	Total resource	Extension sub-area <sup>1</sup>
feet	billion barrels	billion barrels
0-5	*	0.0
5-20	0.1	*
20-40	10.5	2.2
40-60	19.4	1.9
60-80	10.5	0.7
80-100	14.9	4.5
100-130	13.5	1.1
Total	69.0	10.5

<sup>&</sup>lt;sup>1</sup>Included in tota

Note: Totals may not equal sum of components because of independent rounding GPT = gallons of shale oil per ton of rock (42 gallons/barrel)

**Table 6.** The Uinta Basin's potential economic oil-shale resource.

Constraints: at least 25 GPT, at least 5 feet thick, under less than 3000 feet of cover, not in conflict with conventional oil and gas operations, located only on BLM, state trust, private, and tribal lands.

Thickness	Total resource
feet	billion barrels
5-20	5.3
20-40	18.2
40-60	19.4
60-80	11.6
80-100	12.3
100-130	9.9
Total	76.7

Note: Totals may not equal sum of components because of independent rounding GPT = gallons of shale oil per ton of rock (42 gallons/barrel)

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# **Appendix**

**APPENDIX.** Oil-shale resource data for coreholes used in this study. Depths and thicknesses are in feet

Depths and thicknesses are in feel	es are ın	teet						•					•						•			
API USGS#		Type of Log	Twn	Rng 5	Sec M	Mrd U	UTM E	UTMN	Elevation	Mahogany Bed	5	50 GPT Zone		35	35 GPT Zone		25 (	25 GPT Zone		15 GI	15 GPT Zone	
	Den	Fischer Son Assav							Ground	Depth to bed	Ton	Bottom	Thick-	Ton		Thick-	Ton		Thick-	Ton	T Bottom	Thick-
4304730384			1S	1E	33 L	N. Se		4467525	5314	8255	do		0.0	8255.0	8255.5	0.5	8253.0	8257.5			8272.5	36.0
4301330190		×	18	1W				4467149	5427	8002			0.0	7999.5	8007.5	8.0	7992.0	8017.0			8047.5	93.0
4301330083	×		S	2W	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	is is	78246	4468449	5571	8287	0.0470	5 11 5	0.0	8286.0	8288.0	2.0	8281.5	8290.0			8304.0	26.5
4301330060		× ×	s s	v 4 W X			561246	446 / 43 I 446 8 8 4 7	6425	8939	8040.0	8041.3	0.0	8938.0	8940.0	2.0	8929.3	8950.5	21.5	0.619.0	0.0968	51.0
4304730169		×	2S	Ξ			1414	4465415	5294	7452			0.0	7448.5	7457.0	8.5	7442.5	7474.0			7506.0	105.5
4304730774	×		2S	Ξ!			98151	4463089	5068	7071	,		0.0	7065.5	7076.0	10.5	7057.5	7093.0			7116.5	103.5
4304730198	×		58 50	E			96564	4457605	4991	6424	6421.5	6426.0	5.4	6419.5	6433.5	14.0	6412.5	6471.5			5506.0	191.0
4301330226	,	×	\$7	× 1	ر د د	NO NO	95678	4465589	5021	96//			0.0	0.7511	0.6677	C. A	0./4//	6807.0			/811.0	0.09
4304/30220	× ×		2 Z	<u> </u>			33714	1450428	5053	0880			0.0	6646.0	0882.0	0. K	6638.0	0897.0			6681.5	49.5 5
4301330783	· ×		2S	. M			32159	4459519	5100	6647			0.0	6645.5	6649.5	4.0	6642.5	6654.5			5691.5	56.0
4304730186	×		2S	2E			3202	4461428	5135	6833			0.0	6827.5	6837.0	9.5	6824.0	6853.0			5881.5	0.62
4301330061	×		2S	2W	16 U		. 2488	4462196	5650	7307	7305.0	7308.0	3.0	7303.0	7310.5	7.5	7301.0	7323.5			7358.5	93.0
4301330117		×	2S	3W			57824	4465830	6001	8183	8183.0	8184.0	1.0	8179.0	8185.0	0.9	8173.0	8188.5		8161.0	8198.0	37.0
4301330122	×		S 5	3W	77	NO Z	5/0/4	4460322	2834	421/	3 0003	0 2003	0.0	0.000	50205	0.0	517.5	7158.5			7185.5	34.5
4304730254	< >		2 2	w C	, 6		. 51116	4450725	7070	5023	51160	5123.0	. t	5110.0	5120.0	10.0	5110.0	5161.5			5021.0	01.5
4301330786	< ×		S S	2W			578909	4455194	5334	6004	6002.5	0.6216	3.5	6001.5	6010.0	8.5	5997.5	6016.0			5027.5	51.0
4301330094	: ×		38	3W			70267	4452310	5208	5381	5381.0	5381.5	0.5	5378.0	5383.0	5.0	5378.0	5389.5			5403.5	31.0
4301330380		×	38	M9		UN 5	-	4453829	6264	5559			0.0	5556.0	5563.0	7.0	5551.0	5566.5			5582.0	43.5
4301330298	×		38	M9				4450840	5845	4760			0.0	4759.5	4762.5	3.0	4747.5	4774.5			1834.5	89.5
4304731936	×		4S	1E			-	4442476	5270	4049	4047.5	4051.5	4.0	4046.0	4058.0	12.0	4042.0	4071.0			1083.5	73.0
4304733541	×		4S	Ξ.			599059	4440655	5068	3711	3710.0	3717.5	7.5	3706.5	3725.5	19.0	3704.0	3743.5			3740.0	105.5
4301330113	×		4 t	<u> </u>		e e	. 1684	4446150	5167	67.55	0.07.04	45/5.5	0.0	45/2.0	45/9.0	0.7	4568.5	458/.5			0.660	0.40 0.40
4301331010	× ×		4 4 V A	<u>*</u>	23 - 1		588103	4440829	5070	3563	3562 5	3564.5	0.4	3561 5	3570.5	0.0	3557.5	3581.0			3604.0	67.5
4301333635	< >		t 4	WC MC			. C87777	1440775	5354	3491	3491.0	3491.5	2.0	3487.0	3493.0	0.0	3484 5	3500.5			3514.5	51.0
4301331864	: ×		2 4 S	2W.			30991	4441089	5264	3563	3561.0	3565.0	4.0	3556.5	3570.5	14.0	3555.5	3584.0			3599.5	68.0
4301330769	×		48	3W			571332	1440191	5578	3316	3316.0	3316.5	0.5	3315.0	3318.0	3.0	3309.0	3322.5			3327.5	28.5
4301331935	×		4S	3W			98099	4437836	5822	2933	2932.0	2934.0	2.0	2930.0	2935.5	5.5	2927.0	2940.5			2954.0	27.0
4301330414	×		8 5 S 5	<b>₩</b>			559843	4444595	5643	4125	2 0000	2 0000	0.0	4124.0	4125.0	1.0	4122.5	4126.0			4134.0	12.0
4301330838	× ×		2 4 V A	* }	0 C		787766	4445152	2809	3594	3593.5	3595.0	1.0	3591.0	3507.0	C. 4	3590.5	3603.0			3608.0	38.5
4301330444	< ×		2 4 S	. M9			8703	4441689	6771	2480	2479.5	2481.5	2.0	2477.0	2484.0	7.0	2473.5	2489.5			2499.0	37.0
4301330016	: ×		4S	×			12324	4439412	6468	1584	1582.5	1587.0	4.5	1581.0	1590.5	9.5	1561.0	1594.0			1616.5	73.0
4304730175		×	5S	19E	28		1735	4466835	5186	6901			0.0	6896.5	6904.0	7.5	5'9689	6918.0			5950.5	65.5
4304733710	×		5S	3E	); 9		11612	4437308	4730	3096	3088.5	3099.0	10.5	3087.0	3120.0	33.0	3059.0	3128.5		2962.5	3146.5	184.0
4301330823	×;		SS	3.8	⊃ ; ~ ч	NO ZE	, 6893	4435633	6006	3012	3012.0	3014.0	2.0	3010.5	3017.0	6.5	3005.5	3023.0			3038.0	40.5
4301330783	< ×		S S	3W			565710	4433207	6212	2932	2936.0	2942.0	6.0	2935.5	2949.5	14.0	2930.5	2955 5		2918.5	5 696	51.0
4301331575	: ×		5S	3W			. 7773	4429638	6480	2816	2811.5	2820.5	9.0	2808.0	2826.0	18.0	2805.0	2834.0			2848.5	57.5
4301330756	×		5S	4W			, 02009	4435592	6105	2792	2790.0	2795.0	5.0	2789.5	2801.5	12.0	2781.5	2805.5			2825.5	50.0
4301332586	×		5S	4W			9316	4433097	6227	2692	2689.0	2694.5	5.5	2686.5	2700.5	14.0	2680.5	2705.0			2723.5	49.5
4301331815	×		5S	4W			1741	4428396	6372	2416	2411.0	2417.5	6.5	2408.0	2427.5	19.5	2404.5	2436.0			2458.5	63.0
4301330541	×		SS	WS.	4 ; 		0436	4432804	6406	2411	2408.5	2414.5	0.9	2407.0	2423.0	16.0	2402.5	2425.5			2446.0	55.5
45015555/9	× >		200	M C		N W	7664	1472387	10//	1614	5.0072	2/11.3	0.0	1610.0	1625.0	15.0	1604 5	1620.0			5/20.5	50.0
+301332737 U181	<	×	SS	. M8			0121	4433058	6635	246	243.5	250.5	7.0	242.0	258.5	16.5	235.0	259.5		233.5	284.5	51.0
U172		×	5S	8W			6652	4430457	7217	225	223.5	225.5	2.0	221.0	228.5	7.5	221.0	238.5			254.0	33.0
4304730777	×		S9	19E	41	)9 TS	. 62951	4460783	5148	6662	6661.0	6662.5	1.5	6654.5	6667.5	13.0	6652.5	6.9899	_		6708.0	0.96
4304730155	×		S9	20E			15304	4462172	4966	5727			0.0			0.0	5724.5	5727.5			5737.5	17.5
4304731571		×	89	21E	28		21813	4458242	4961	5040		1	0.0			0.0	5039.0	5040.0		5034.5	5054.5	20.0
4301333581	×		S9	₩ ₩			00001	4426942	6679	2254	2252.0	2255.0	3.0	2248.0	2263.0	15.0	2242.5	2271.5			2293.5	62.5
4301330405	×		S S	4 W	23	NO NO	559325	4421669	08/90	1798	1795.0	1,56.5	3.0	1703.5	1816.5	0.01	1790.0	1873.0	33.0	1779 0	1834 5	39.5 55.5
4301cc10c+	<		2	, , ,			· · · · · · · · · · · · · · · · · · ·	47777	larc/	06/1	177.0	1000.0	7.11	1,73.5	1010.7	7.7.7	1,70.0	0.0701	_		C+10	J., J

APPENDIX	K continued	pəi								]												
API	# SDSN	Type of Log	Twn	Rng S	Sec M	Mrd U	UTM E	N MIN	Elevation	Mahogany Bed	5.	50 GPT Zone		35	5 GPT Zone		25 (	GPT Zone		15 G	GPT Zone	
		Fischer Den Son Assay							Ground	Depth to bed	Top	Bottom	Thick- ness	Top	Bottom	Thick- ness	Top	Bottom	Thick- ness	Top	T Bottom	Thick- ness
4301330496		x		5W	21 U	NN S		4422129	0.00	1798	1795.0	0.1081	6.0			18.0	1790.0	1823.0	33.0			55.5
4304/31018 4304731381		× ×	S 25					445 <i>2</i> 081 4447534	4830	5152 4404			0.0	4400.5	5152.5 4409.0	8.5	5147.0 4394.0	4421.0	27.0	3143.5 4368.5	4439.5	71.0
4304733575		×		22E	25 S	9 TS	636669	4448686	5503	4149			0.0			0.0	4144.5	4156.0	5.0			34.0
4301330770		· ×	•					4437612	5532	3167	3165.5		3.0			7.0	3164.0	3179.0	15.0			42.0
4301331372		× ×		16E	28 32 8 S	SE	574589	4437016	5618	3082	3106.0		3.0			5.5 5.5	3096.5	3092 5	15.5			42.0
4301331508		< ×	S8				579457	4435643	5367	2931	2928.5	2934.0	5.5	2927.5	2941.5	14.0	2924.0	2951.5	27.5			71.5
4301330690		×	88 88				583320	4439272	5266	3376	3373.0		6.0			17.0	3363.5	3400.5	37.0			75.5
4301333013		× ×	× ×	1/E 17E	25 25	2 2	582180	4436019	5249	3015	3190.5		0.0 0.0			16.5	3183.0	32.14.5	31.5	3154.0		50.5 79.0
4304736188		< ×	8 8 8 8					4439383	4980	3354	3352.5		2.5		3359.5	10.0	3347.0	3374.0	27.0			62.0
4304731116		×				ST S		4436146	4930	3066	3064.0		4.0			13.5	3058.0	3085.0	27.0	2 1100		66.5
4304/31345		× ×		18E 20E	36 15 S		598192 614534	4436204 4442239	4831	3576	3572.0		10.0			35.0	3532.0	3641.0	31.0	3400.5		76.5 253.5
4304733421							617917	4437124	4661	2963	2959.0	2966.5	7.5			28.0	2925.5	3007.0	81.5	2750.0		285.5
4304733794		× ×	S & &	21E 21F	- 5 S S	SIT	627733	4445434	5167	3434			0.0	3430.5	3434.0	3.5	3425.5	3435.0	9.5	3417.0	3453.5	36.5
4304731609		< ×					622983	4442058	4750	3413	3412.0		3.5			24.5	3399.5	3469.5	70.0	3270.5		221.5
4304731065		×					620216	4439938	4682	3314	3312.5		5.5			17.0	3278.5	3357.5	79.0	3146.0		243.0
4304731604		× ×	x x	21E	21 22 8	9 5 5 5	622232	4440822	4703	3316	3314.0		7.5			29.0	3273.5	3380.5	107.0	3196.0		249.0
4304731253		< ×						4440529	4819	3228	3225.0		7.5			34.0	3186.0	3298.5	112.5	2926.5		374.5
4304733746		×						4437545	4699	3054	3050.5		8.0			28.0	3009.5	3094.5	85.0	2880.0		250.0
4304733252		× >		21E	36 36 36	9 9 7 5	628094	4438025	4759	2914	2910.0	2920.0	10.0			38.0	2870.0	2992.0	122.0	2800.0		400.0
4304731810		< ×						4443416	5036	3705	2007		0.0			3.0	3698.5	3708.5	10.0	3663.0		114.0
4304734710		×	88					4441795	5052	3491			0.0			13.5	3487.0	3532.0	45.0	3383.0		177.0
4304731355		×		22E	20 S	o s ST	630418	4440611	4793	3163	3162.5		3.5			31.5	3129.0	3204.0	0.50	3056.5		214.0
4304733583		< ×						4436875	4715	2771	2767.0		0.7			31.0	2728.5	2815.5	87.0	2560.5		320.3 293.0
4304734210		: ×			35 S			4436993	4880	2837	2833.0		10.5			34.0	2792.5	2891.0	98.5	2586.0	2924.5	338.5
4304734085		×;	88 s	23E		9 Ts	639172	4439428	4899	2946	2941.5	2949.5	8.0			34.5	2908.0	3009.5	101.5	2661.0		365.0
4304736061		< ×						4438266	5076	2799	2794.5		10.0			33.5	2754.0	2851.5	97.5	2627.5		337.5
4304732106		×						4445356	5518	2935			0.0			0.0	2931.0	2937.5	6.5	2918.0		46.0
4304732260		×	S ×	25E 25E	2 5 S S	o s S Is	059579	4446649	5637	2798	1463.5		0.0	2797.5	2799.0	1.5	2794.5	2810.5	16.0	2786.0		68.0
4301330997		· ×						4435024	5992	3003	2999.5		8.0			17.5	2991.0	3020.0	29.0	2959.0		72.5
4301331479		×	S6	15E		SL	568546	4431488	6217	2928	2924.0		7.5			18.0	2915.5	2944.0	28.5	2906.0	2963.0	57.0
4301330446		× ×	8 8 8	10E	29 S			4428709	5581	2808	7888.0		0.0			2.5	2797.5	2816.5	19.0	2790.0		‡ 4 ë e
4301331425		×						4434058	9905	2785	2781.5		7.0			18.5	2768.5	2804.0	35.5	2734.0		105.0
4301330926		× >	S6	17E			581764	4433587	5279	2803	2801.0	2805.5	4.5 5.0			10.5	2796.0	2817.5	21.5	2795.5		40.5
4301330552		< ×	98	17E				4431996	5243	2671	2668.5		5.4 5.5			13.0	2664.5	2695.5	31.0	2654.0		64.0
4301332787		×						4429669	5212	2440	2437.0		5.5			16.0	2430.0	2461.5	31.5	2405.5		69.5
4301330601		×						4428750	5520	2493	2490.0		6.0			15.5	2484.0	2517.0	33.0	2474.0		65.5
4304/35/75		× ×	8 8 8 8	18E 19E	7 O	S S	59/049 603012	4432650	483/	2692	2688.5		5.0 6.0		2711.0	25.5	3020.5 2663.0	3046.5 2722.5	26.0	2578.0	2731.0	04.3 153.0
4304732457		×	S6	19E				4431670	4649	2522	2518.5		6.5			21.0	2490.5	2541.5	51.0			126.5
4304732227		×;	S6	19E	24 S			4430846	4691	2509	2506.5		5.5			17.5	0.000	0.1000	35.5	0 0200		88.5
4304730749		< ×				ST 0	612958	4435952	4649	2845	2843.0	2849.0	0.0	2842.0	2863.0	21.0	2833.5	2873.5	92.0 40.0	2784.5	2402.0 2898.5	129.0 114.0
4304730434								4433457	4747	2614			5.5			23.0	2579.0	2646.0	67.0	2354.0		318.5
4304/10329	U043	× ×		20E	36 S	SI 0	61968 / 619748	4426886	4824 4941	2420			6.5		2312.0	38.0 18.0	2268.0	2335.5	67.5	1953.5		321.0 403.0
4304734875		×	S6	21E				4434470	4688	2641			8.0		2660.5	29.5	2600.5	2684.5	84.0			358.5
4304/34/4/		× ×		21E 21E		o o SI SI	625111 627413	4434922	4821	2819	2813.0	2825.0 2602.0	19.0	2808.0		53.5	2538.0	2877.5	90.5	2307.5	2900.0 2715.0	386.5 407.5
4304734640		×						4431988	4851	2533	2526.5		12.0			43.5	2498.5	2588.5	0.06	2259.0		342.5
4304734584		× >	86 86	21E	21 25 8	SI	623480	4431229	4875	2472	2465.5	2476.5	11.0		2503.5	41.0	2435.0	2520.5	85.5	2213.5		325.0
		<						-	,	1	1		:	_		<u>-</u>		;				307.5

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UTMAN         Plasel         96.047 Zone         Table Plasel         SO OF Y Zone         Table Plasel         <	Elevation         Bsd           Ground         Depth         Top           level         10 bed         Top           4911         2313         2310.5           5100         2271         2205.           4810         2645         2642.           4798         2755         2750.           4700         2687         2683.           4851         2350         2340.           4851         2350         2340.           4851         2350         2340.           4851         2350         2340.           4851         2350         2342.           2350         2344.         2350.           2350         2345.         2340.           2350         2345.         2340.           2350         2345.         2340.           2350         2345.         2345.           2360         2345.         2345.           2360         2345.         2345.           2360         2345.         2345.           2360         2345.         2345.           2360         2345.         2345.           2360         2360         2345. </th <th>0 GPT Zone TI Bottom 2325.5 2383.5 2217.5 2652.5 2693.0 2432.5 2356.5</th> <th>To 2303.( 2368.: 2201.( 2633.(</th> <th>F</th> <th>25 GPTZ Top Botte</th> <th>Ē</th> <th>15 GPT Zone</th> <th></th>	0 GPT Zone TI Bottom 2325.5 2383.5 2217.5 2652.5 2693.0 2432.5 2356.5	To 2303.( 2368.: 2201.( 2633.(	F	25 GPTZ Top Botte	Ē	15 GPT Zone	
CHORDIS         APARTIS         Tryan         APARTIS         Tryan         Tryan         APARTIS         Tryan         Tryan         APARTIS	Lyola Lephn   Lephn	Bottom 2325.5 2383.5 2217.5 2652.5 2761.5 2693.0 2443.5 2356.5 2356.5	Top 2303.0 2368.5 2201.0 2633.0	7		Ξ		Ē
81.         6.2.9.7.         4.0.1.         27.1.         2.1.0.2.         2.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.         2.0.0.         4.0.0.<	4911         2313         2310.5           4903         2377         2372.5           4810         2210         2265.0           4798         2755         2750.5           4700         2687         2683.0           4859         2426.5         2420.5           4859         2426.5         2440.5           4958         2078         2072.0	2325.5 2383.5 2217.5 2652.5 2761.5 2693.0 2332.5	2303.0 2368.5 2201.0 2633.0					Thick Bottom ness
81.         67.07.9         47.00.         27.00. <td>5100 2210 2205.0 4810 2646 2642.0 4700 2687 2683.0 4861 2692 242.0 4861 2350 244.0 4958 2078 2072.0</td> <td>2217.5 2217.5 2652.5 2761.5 2432.5 2356.5</td> <td>2201.0 2633.0</td> <td></td> <td></td> <td></td> <td></td> <td>382.5</td>	5100 2210 2205.0 4810 2646 2642.0 4700 2687 2683.0 4861 2692 242.0 4861 2350 244.0 4958 2078 2072.0	2217.5 2217.5 2652.5 2761.5 2432.5 2356.5	2201.0 2633.0					382.5
8.1. GANDA         48.00         58.00	4810 2646 2642.0 4798 2755 2750.5 4709 2687 2683.0 4859 2425 2420.5 4861 2350 2344.0 4958 2078 2072.0	2652.5 2761.5 2693.0 2432.5 2356.5	2633.0					2268.5 363.
81         63008         44174         4879         2887         26009         100         5675         3715 <th< td=""><td>4700     2687     2683.0       4859     2425     2420.5       4861     2350     2344.0       4958     2078     2072.0</td><td>2693.0 2432.5 2356.5</td><td>2746.5</td><td></td><td></td><td></td><td></td><td>5</td></th<>	4700     2687     2683.0       4859     2425     2420.5       4861     2350     2344.0       4958     2078     2072.0	2693.0 2432.5 2356.5	2746.5					5
8.1.         CORRES         443741         5447.0 <td>4859 2425 2420.5 4861 2350 2344.0 4958 2078 2072.0</td> <td>2356.5</td> <td>2675.5</td> <td></td> <td></td> <td></td> <td></td> <td>2769.5 339.</td>	4859 2425 2420.5 4861 2350 2344.0 4958 2078 2072.0	2356.5	2675.5					2769.5 339.
SI         GYRNAR 4 42237-3         4066         1006	4958 2072.0		2412.5 2339.5			_		300. 2429.5 379.
SL         CRASS         4966         1966         1966         1966         1966         1966         1966         1966         1966         1966         1966         1966         1966         1966         1966         1967		2086.5	2068.0			-		
C. CARRELLO         STATE CARLES         STATE CARLES </td <td>4965 1966 1964.0</td> <td>2352.0</td> <td>1956.0</td> <td></td> <td></td> <td></td> <td></td> <td>456.</td>	4965 1966 1964.0	2352.0	1956.0					456.
S. C. A. C. A	2236 2231.0	2242.5	2224.0					2
SL         GGGGGG         AGASTAG         SASTAG         SASTAG         AGASTAG         AGASTA	1996 1991.0	2003.5	1985.5					499.
SL         68982         442378         54.6         2240 <t< td=""><td>2097 2092.5</td><td>2107.5</td><td>2085.5</td><td></td><td></td><td></td><td></td><td></td></t<>	2097 2092.5	2107.5	2085.5					
SL         C512-86         5415         5415         5416         5417         5418 <t< td=""><td>5243 2240 2234.0</td><td>2245.0</td><td>2226.0</td><td></td><td></td><td></td><td></td><td>2322.0 338.</td></t<>	5243 2240 2234.0	2245.0	2226.0					2322.0 338.
3.1.         C. 1979.         A. 1979. <th< td=""><td>5115 2318 2312.5</td><td>2323.0</td><td>2304.0</td><td></td><td></td><td></td><td></td><td></td></th<>	5115 2318 2312.5	2323.0	2304.0					
L. G7M77 442278         S. 40         SR. 50         SR. 50 <th< td=""><td>2432 203/ 2034.3</td><td>2040.5</td><td>1055.0</td><td></td><td></td><td></td><td></td><td>399.</td></th<>	2432 203/ 2034.3	2040.5	1055.0					399.
E. G6426.         47578.         579.         1092.         1082.	5004 1963 1961.0	905.5	0.0001					410.
SIGN CASTAN CANADA         SRN CASTAN CANADA	5750 1092 1089.0	1095.5	1086.0					353
S1         G67008         4472348         S871         IOTA         ATA         STA         STA <t< td=""><td>1171 1168 5</td><td>1176.5</td><td>1159.5</td><td></td><td></td><td></td><td></td><td>386</td></t<>	1171 1168 5	1176.5	1159.5					386
SIL         G65859         4418/RSD         588         448         480         485         5         476         300         546         472         500         74         500         74         500         74         500         74         500         74         500         74         74         500         74         74         500         74         74         750         74         74         750         74         74         750         74         750         74         750         74         750         74         750         74         750         74         750         7	5813 1027 1024 0	1031.5	1015.0					1160 0 404
SI, 678847         67897         571         510         519         504         576         576         576         577 <t< td=""><td>5879 481 480.0</td><td>485.0</td><td>476.0</td><td></td><td></td><td></td><td></td><td></td></t<>	5879 481 480.0	485.0	476.0					
SL         GGFTS         FYATOR         STATE         S	516 510.0	519.5	504.5					386
S. 6.08.6. 1. 42.8867         5.81         5.94         5.95         5.94         5.95         5.94         5.95         5.94         5.95	5745 501 495.5	501.5	494.0					327.
S. 5. 588.8         441036         7.36         1957	5871 504 500.5	508.0	492.5					
SL         56881         442384         6544         2334         6744         2334         6743         775         21839         21839         24834         333         2494         775         1895         442384         315         2484         313         2494         31         2413         2480         313         2494         417790         707         710         2472         2473         2	7369 1957 1954.5	1957.5	1951.5					2006.5 70.5
SL         568.54         4427100         7007         7335         2335.0         2337.0         2337.0         2340.0	2167 2163.5	2171.0	2159.5					
SL         579228         442337         670         770         470         77	7077 2335 2335.0	2337.0	2333.0					
SL         578.22         442.59         64.59         2.24.2         2.42.0	6706 1709	0 127	1706.0					1741.0 39.5
SL         5775.22         442.17         648.8         2.21         2.21.0         6.2         2.44.5         2.65.0         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2         1.0         2.45.2	2423 2420.0	2431.0	2414.0					16.0 121.5
SI.         SI. <td>2250 2250.3</td> <td>2251.0</td> <td>2245.5</td> <td></td> <td></td> <td></td> <td></td> <td></td>	2250 2250.3	2251.0	2245.5					
SL         583398         4271115         5990         2033         20225         50425         1410         2045         1450         2045         1450         2045         1450         2045         20425         140         2045         20445         2045	5866 2352 2345.5	2355.5	2344.5					
S1         591469         4424105         5318         2120         2115.0         2115.5         9.5         2113.5         2143.5         30.5         208.5         2145.0         85.0         30.7         2145.0         85.0         422868         80.0         182.1         182.5         182.0         182.5         182.5         183.4         18.0         179.0         183.4         35.0         183.4         35.0         183.4         35.0         183.4         35.0         183.4         35.0         183.4         35.0         187.5         187.5         187.0         188.4         187.5 <td>5950 2033 2029.5</td> <td>2034.5</td> <td>2028.5</td> <td></td> <td></td> <td></td> <td></td> <td></td>	5950 2033 2029.5	2034.5	2028.5					
S1         594622         4422868         5078         1823         1820	2120 2116.0	2125.5	2113.0					
SL         597108         442367         509         1928         1925.0         1931.0         60         1921.5         1906.5         290.0         200.0         1921.0         4534.0         1906.0         1924.0         1906.0         1921.0         1906.0         1921.5         1906.0         200.0         200.0         1910.0         55.2         200.0         1900.0         200.0         200.0         1910.0         55.2         1927.5         1907.5         1807.0         1800.0         400.0         1800.0 </td <td>5078 1823 1820.0</td> <td>1828.0</td> <td>1816.5</td> <td></td> <td></td> <td></td> <td></td> <td></td>	5078 1823 1820.0	1828.0	1816.5					
SIL         607303         4425331         4987         2234         2231,0         22375         2247.5         200,0         2209,5         2234,2         43.5         2034,0         210,0         2234,2         43.5         2180,0         2234,2         43.5         2030,0         210,0         2234,2         43.5         2180,0         200,4         2234,2         43.5         200,4         2234,2         43.5         200,4         220,4         43.5         2180,0         200,4         23.5         200,4	5079 1928 1925.0	1931.0	1921.5					118.0
SL         608962         4423647         5095         2099         2010         5.5         2003.0         2110.5         17.5         2074.5         2118.0         49.5         17.5         17.5         17.5         17.8         17.5	4987 2231.0	2237.5	2227.5					
SL         603469         4422194         5057         1812         186.0         185.0         70         1862.5         182.5         180.0         185.0         70         180.5         182.5         180.0         180.0         180.5         180.0         180.5         180.0         180.5         180.0         180.5         180.0<	5095 2099 2095.5	2101.0	2093.0					0
SL         607333         4421475         5210         1956         195.         1942.         1959.5         170         1999.6         41.5         186.0         41.5         1899.5         170         1999.6         41.5         186.0         41.5         188.0         41.5         188.0         41.5         188.0         41.5         18.6         41.5         18.6         41.5         18.6         41.5         18.6         41.5 </td <td>5057 1812 1808.0</td> <td>1815.0</td> <td>1805.5</td> <td></td> <td></td> <td></td> <td></td> <td>1853.5 118.</td>	5057 1812 1808.0	1815.0	1805.5					1853.5 118.
SL         605763         4418769         5263         1664         1673.0         8.5         1660.0         1686.5         265         1669         1686.3         1659         1691.5         5263         1588.0           SL         600968         4418188         5362         1726         1726.0         40.0         1735.0         160.0         1735.0         1749.0         33.5         1680.0           SL         610916         442536         4868         2082         2011.5         20         2000.0         14.0         2072.5         1040.0         31.5         1040.0         31.5         1080.5         32.5         1050.0         2004.0         2005.0         1004.0         2004.0	5210 1950 1947.0	1952.5	1942.5					
SL         60798         4418188         5362         1724         17240         1728.0         40         1715.0         1745.0         1735.0         1749.0         1745.0         1745.0         1749.0         1745.0         1749.0         1745.0         1749.0         33.5         1688.0           SL         610916         4425369         4868         2079.2         2079.2         2075.0         2076.0         140         2072.5         2144.0         33.5         16820           SL         610956         442157         5195         1829.0         1829.5         1829.5         1829.6         1	5263 1668 1664.5	1673.0	1660.0					
SL         610916         44223549         2082         2079,0         2083.5         4.4         2075,0         2014,0         31.5         2011,0         31.5         2011,0           SL         610956         4422724         5093         2019,0         2011,5         2076         2004,0         2028,5         2104,0         31.5         1800.5           SL         610956         4421737         5097         2019         2022,5         2012,5         2012,5         2020,0         3.0         1820,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         1800,0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0         3.0 </td <td>5362 1726 1724.0</td> <td>1728.0</td> <td>1719.0</td> <td></td> <td></td> <td></td> <td></td> <td>1768.0 100.</td>	5362 1726 1724.0	1728.0	1719.0					1768.0 100.
SL         611826         4427274         5093         2011         2009-5         2011.5         20         2015.5         80         2015.5         2015.5         80         2015.5         80         2015.5         80         2015.5         80         2015.5         80         2015.5         80         2015.5         80         30         1829.6         44215.3         30         30         30         1829.6         30	4868 2082 2079.0	2083.5	2076.0					
SL         610956         4421537         5155         1829         18295         0.5         18290         18290         18295         0.5         18290         18290         18295         0.5         18290         18290         18290         18290         18290         18290         18290         18290         18290         18290         18290         18290         18295         3.5         18290         18290         3.5         18290         18290         3.5         18290         3.5         18290         3.5         18290         3.5         18290         3.5         18290         3.5         3.5         18290         3.5         18290         3.5         3.5         3.5         3.5         3.5         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.0         3.5         3.5         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.6         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2         3.2	5093 2010 2009.5	2011.5	2007.5					2044.0 63.
SL         6.226.75         44244343         506/         2019         2016.0         2022.5         2022.0         193.0         1934.0         244.55         193.0         203.5         193.5         193.0	1829 1829.0	1829.5	1829.0					107.0
SL         623845         4424560         5076         2044         2040         2050         100         2036.5         208.5         32.0         1975.5         1991.0         15.5         1993.5         62.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.5         1903.0         1803.0         1803.0         1803.5         1803	2019 2016.0	2022.5	2012.5					
SL         619499         4423304         5077         1980         1977         1982.0         50         1975.5         1991.0         155         1994.5         1994.5         1994.5         1994.6         1894.0         1855         1994.0         1855         1994.0         1855         1894.0         1872.0         1875.5         1994.5         1994.5         1894.0         1872.0         1870.0         1872.0         1875.5         1894.0         1894.0         1884.0         1885.0         1875.5         1895.5         1995.0         1875.5         1895.0         1757.5         1875.5         1895.0         1757.5         1875.0         1875.0         1875.5         1895.0         1757.5         1875.0         1875.5         1895.0         1757.5         1875.0         1875.5         1895.0         1875.5         1885.5         1985.0         1875.0         1875.0         1895.0         1757.5         1895.0         1875.5         1885.	2045 2040.0	2050.0	2036.5					0
SL         676428         4420189         5356         1850         1884.0         1854.0         6.0         1842.0         1860.0         1870.0         1872.0         575.2         1757.5           SL         635938         4417399         5345         1644         1642.0         1646.5         4.5         1641.5         1656.5         15.0         1820.0         1872.0         1872.5         1872.0         1875.2         15.0         1872.5         1669.5         48.0         1757.5         1757.5         1757.5         1757.5         1875.5	1980 1977.0	1982.0	1975.5					
SL         619938         4412389         5345         1644         1864.5         45         1641.5         1666.5         18.0         48.0         48.0           SL         637584         442684         5067         1864         1876.0         1976.2         1976.5         1901.5         49.0         1787.0         1899.5         11.25         1535.5           SL         637584         442688         5192         1887.0         1990.0         1875.2         1901.5         49.0         1787.0         1940.0         1976.3         1976.2         2040.0         94.0         1694.0         1694.0         1694.0         1694.0         1887.2         160.1         1897.2         1694.0         1694.0         1897.2         1694.0 </td <td>5356 1850 1848.0</td> <td>1854.0</td> <td>1842.0</td> <td></td> <td></td> <td></td> <td></td> <td>1899.0 141.5</td>	5356 1850 1848.0	1854.0	1842.0					1899.0 141.5
SL         635056         4425645         5067         1864         1873.0         1877.0         190.1         1852.5         1901.5         490.1         1889.5         112.5         1553.5           SL         631728         4426845         4908         1986         1986.0         1999.0         13.0         1976.5         2019.5         43.0         1946.0         2040.0         94.0         1694.0           SL         637584         4424848         5192         1887         1882.5         16.0         1846.5         1882.5         46.0         1818.0         1921.5         103.5           SL         633509         4423667         5243         1786         1786.0         1774.0         1817.0         487.5         1977.5         90.0           SL         633509         4423667         5243         1936         1924.5         14.5         1960.5         40.5         1887.5         1977.5         90.0           SL         639120         442360         503         1817         1812.0         1877.0         1807.5         37.0         1887.5         90.0           SL         63810         442030         4893         126.0         1274.0         1209.5	5345 1644 1642.0	1646.5	1641.5					144.
SL         631728         4426845         4908         1986         1986.0         1999.0         13.0         1976.5         2019.5         43.0         1946.0         2040.0         94.0         1694.0           SL         637584         4424888         5192         1857         1852.5         1868.5         16.0         1846.5         1892.5         46.0         1818.0         1921.5         10.3	5067 1864 1858.0	1877.0	1852.5	,		_		1927.0 373.
SL         637584         4424888         5192         1857         1852.5         1868.5         160         1846.5         1892.5         460         1818.0         1921.5         103.5           SL         637451         4424388         5295         1785         1780.0         1796.0         160         1774.0         1817.0         43.0         1921.5         103.5         139.5           SL         639360         442360         50.4         1812.0         1823.0         11.0         1807.5         1887.5         1977.5         93.0           SL         63810         442030         489         1826         1274.0         180.5         1844.5         37.0         1781.5         1863.5         82.0           SL         63810         442030         489         136         1274.0         1275.0         1290.5         33.5         1286.0         137.5         1040.0           SL         62961         441086         4970         1314         1310.5         1323.0         1759.5         1780.0         1379.5         1379.5         1379.5         1379.5         1379.5         1494.0	4908 1986.0	1999.0	1976.5				•	2052.0 358.
SL         637451         4422858         5295         1786         1780         1796.0         160         17740         1817.0         43.0         1721.0         1814.0         93.0         1539.5           SL         629350         442360         5243         1936         1928.0         192.5         14.5         1920.0         1960.5         40.5         1887.5         1977.5         90.0           SL         639100         442360         50.3         1817         1812.0         1823.0         11.0         1807.5         1844.5         37.0         1781.5         1863.5         82.0           SL         634402         4420406         4970         1314         1310.5         133.0         125.0         1250.4         1290.5         35.0         1387.5         71.5         1040.0           SL         629617         4410861         5369         1766         1763.5         1771.0         7.5         1789.5         1789.5         1794.0         54.5         1666.0	5192 1857 1852.5	1868.5	1846.5	-				
SL         633509         4423667         5243         1936         1928.0         1942.5         145         1920.0         1960.5         40.5         1887.5         1977.5         90.0           SL         639102         4423509         863         1817         1812.0         1823.0         11.0         1807.5         1844.5         37.0         1781.5         1863.5         82.0           SL         638102         442203         4893         1266         1262.0         1274.0         1257.0         1290.3         33.5         1280.0         1317.0         89.0           SL         624429         4420406         4970         1314         1310.5         1323.0         125.0         1789.5         1386.0         1357.5         71.5         1094.0           SL         629617         4419861         5369         1766         1763.5         1771.0         7.5         1789.6         1789.5         1794.0         54.5         1666.0	1785 1780.0	1796.0	1774.0	•				1842.5 303.0
SL 639032 4425309 5030 1817 1812.0 1825.0 11.0 1807.5 1844.5 37.0 1781.5 1863.5 82.0  SL 638100 4422030 4893 1266 1262.0 1274.0 125.0 1257.0 1290.5 33.5 1228.0 1317.0 89.0  SL 63492 4420406 4970 1314 1310.5 1323.0 125 1304.5 1395.5 35.0 1286.0 1357.5 71.5 1094.0  SL 629617 4419861 5369 1766 1763.5 1771.0 7.5 1759.5 1781.0 21.5 1739.5 1739.5 1794.0 54.5 1666.0	1930 1928.0	1942.5	1920.0					293.
SL 638110 4422030 4893 1266 1262.0 1274.0 12.0 1257.0 1290.5 33.5 1228.0 1317.0 89.0 SL 634492 4420406 4970 1314 1310.5 1323.0 12.5 1304.5 1339.5 35.0 1286.0 1357.5 71.5 1094.0 SL 629617 4419861 5369 1766 1763.5 1771.0 7.5 1759.5 1781.0 21.5 1739.5 1794.0 54.5 1666.0	5030 1817 1812.0	1823.0	1807.5					267.
SL 624672 4420406 4970 1314 1310,3 1325,0 12,3 1304,3 1339,3 55,0 1286,0 137,3 71,3 1094,0 SL 629617 4419861 5369 1766 1763,5 1771,0 7.5 1759,5 1781,0 21,5 1739,5 1794,0 54,5 1666.0	4893 1266 1262.0	1274.0	1257.0					290.0
SL 02901/ 4419601 5309 1/00 1/03:3 1//1:0 /.3 1/39:3 1/61:0 21:3 1/39:3 1/94:0 34:3 1000:0	49/0 1314 1310.5 1	1323.0	1304.5					1368.0 2/4.
	5369 1/66 1/63.5	0.1//1	5.66/1					

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API USGS	#	Tyne of Log	LW.	Rng	Sec Mrd	MTU	THE	Elevation	Mahogany	3	50 GPT Zone		35	35 GPT Zone		25.0	25 GPT Zone		15.0	15 GPT Zone	
		Fischer							Depth	E	-	Ī	Ė	1	Thick-	Ę	.	Thick-	E	.	Thick-
4304735745		oon Assay	501	73F	12	646718	4426654	1evel 542.6	1904	1899 5	1913 5	14.0	1803 O	1942 5	10 SS	1859 5	1969 O	100 5	10b	Bottom	342 5
4304735030	< ×			23E			4425844	5311	1865	1861.5	1880.0	18.5	1852.0	1903.0	51.0	1793.5	1904.0	110.5			345.5
4304734770	×			23E	S SI		_	5278	1923	1919.5	1932.0	12.5	1913.5	1959.0	45.5	1885.0	0.9861	101.0			300.0
4304734728	×						4425372	5334	1795	1790.5	1806.0	15.0	1789.5	1834.5	45.0	1728.0	1837.5	109.5			342.5
4304734773	×						4425054	5437	1830	1824.0	1841.5	17.5	1817.5	1864.5	47.0	1789.0	1895.5	106.5	1563.5	1896.5	333.0
4304735721	×		S01	23E	75 5 81 4	63965	4423800	5332	1843	1838.0	1855.0	17.0	1833.0	1876.0	43.0	1773.5	1874.5	101.0	0.3161	2 00 21	316.0
4504/30280		×			-		4423293	5292	795	792.5	801.0	20.0	784.5	821.0	36.5	756.0	854.0	0.511	478.0	863.5	385.5
U052	2 2	< ×					4422663	5061	963	958.5	972.5	14.0	952.0	992.0	40.0	928.0	1033.5	105.5	ò	9	428.0
U128	8	×					4421741	5219	935	932.0	948.0	16.0	924.0	970.5	46.5			127.5			485.5
U049	6	×					4422104		887	882.0	891.0	9.0	876.0	0.806	32.0	850.5	945.5	95.0			362.0
U047	7	×		•			4420958		856	854.0	867.0	13.0	846.0	878.5	32.5	815.5	907.5	92.0	568.5	919.0	350.5
U051	1	×					4420690		1051	1046.0	1059.5	13.5	1043.0	1085.0	42.0	1016.0	1116.5	100.5			407.5
4304733165	×						4419562	5067	812	807.0	825.0	18.0	785.5	831.5	46.0	749.5	863.5	114.0	567.5	1030.0	462.5
U050 11060		×					4419210	5432	882	878.0	893.5	15.5	871.5	914.0	42.5	846.0	941.5	95.5			387.5
U089	6 -	×					4419422	5580	699	0.999	6/3.5	ć./	0.099	68/.5	27.5	635.0	0.617	80.0	0	9	310.5
0035	0 4	× ;	201	75E	4 C	06141	5777777	0169	405	401.5	410.5	9.0	597.5	192 5	0.62	3 /0.0	451.0	0.18	138.0	275.5	343.0
11037	0 1	< >					4423613	6340	105	100.0	108.0	0.7	0.25.0	122.5	2, 4, 5	68.5	142.5	74.0	0.0	3240	3240
11048	. 0	< >					4423173	5435	818	515.0	523.5	, x	508.0	541 5	33.5	482.0	5.44 5	2.5	376.0	602 5	316.5
U139	. 6	: ×					4421647	5720	467	464.0	472.5	8.5	457.0	486.5	29.5	431.0	514.0	83.0			318.5
U038	8	×					4420198	6173	393	385.0	394.5	9.5	382.5	411.5	29.0	360.0	437.5	77.5	150.0	448.0	298.0
U029	6	X					7 4418774	5746	637	632.5	643.0	10.5	626.0	659.5	33.5	603.5	692.0	88.5	383.0	712.5	329.5
U138	8	×			34 SL		4418409		165	162.0	169.5	7.5	158.0	180.5	22.5	136.0	198.0	62.0			231.0
4301332453	×			16E	2 SL		4415467	6258	1783			0.0	1783.0	1784.0	1.0	1790.0	1799.5	9.5	1775.5	1807.0	31.5
4301331994	×						4413141	6501	1739			0.0	1738.5	1740.5	2.0	1730.0	1743.5	13.5	1714.0	1767.5	53.5
4304731108	×						4414178	5605	1565	1564.5	1567.5	3.0	1562.5	1571.0	8.5	1557.0	1589.5	32.5	1526.5	1612.0	85.5
4304/3690/ 4304731178	×	,	211	19E	17 ST	L 601943	4412955	5/11	1544	1356.5	1247.5	8.0	5.55.1	1258.5	16.0	1329.5	15/4.0	2. ts	1486.5	0.5951	108.5
4304731178	>	<		20E			4415740	7955	1638	1636.0	1638.5	2.5	1633.0	1643.5	10.5	1632 5	1658.0	25.5	1604 0	1681.0	77.0
4304734774	< ×			22E	4 SL		4417007	5593	1682	1679.0	1686.0	7.0	1676.0	1696.0	20.0	1655.5	1708.5	53.0	1574.5	1727.5	153.0
4304731067	×			22E		L 62950]	4414181	2608	1514	1512.0	1516.0	4.0	1507.5	1522.0	14.5	1501.0	1537.0	36.0	1434.5	1540.5	106.0
4304734775	×					L 631920	4415390	9899	1632	1629.0	1634.0	5.0	1626.0	1645.5	19.5	1604.5	1654.0	49.5	1540.5	1677.0	136.5
4304732840	×						3 4410149	6909	1502	1498.0	1504.5	6.5	1494.0	1513.0	19.0	1488.5	1532.0	43.5	1430.0	1549.5	119.5
4304734371	×						4414970	6111	1668	1664.5	1673.5	9.0	1664.5	1694.0	29.5	1638.0	1699.5	61.5	1525.0	1718.5	193.5
4304/34252	× ;		211	73E	10 SE	043308	4414792	1896	1111	044.5	0.0111	0.6	040.5	0.6211	27.5	1080.5	070 5	0.79	913.0	0.6611	246.0
4304732853	× ×						4409310	5941	804 408	800.0	809.0	9.0	800.5	831.5	31.0	773.0	838.0	65.0	642.5	853.5	211.0
980N		×					4415339		581	577.0	591.5	14.5	572.5	608.5	36.0	553.0	624.5	71.5	355.0	624.0	269.0
U025	2	×					4414357		518	516.5	527.5	11.0	509.5	540.0	30.5			60.5			228.0
N088	× ·	×					4408591	6130	349	343.0		6.5	340.0	363.0	23.0	322.5	377.5	55.0			207.0
U032		×	SII	25E	3 ST		4417093	6339	406	403.0	412.5	9.5	396.5	424.5	28.0	374.5	448.0	73.5	183.0	459.5	276.5
1113	7	× ×			3 2	7,00000 7	4410933	6700	644	87.0		2./1	82.0	105.5	23.5	61.0	119.0	58.0	00	222.0	222.0
U033		: ×					4413814	5905	383	380.5		8.5	377.0	409.5	32.5	357.0	429.0	72.0	156.0	431.5	275.5
U034	4	×		` '			4413059		382	377.5	386.0	8.5	371.5	395.0	23.5	351.0	409.0	58.0	206.0	426.0	220.0
U149	6	×					4413046		418	414.0		7.5	409.5	436.5	27.0	386.0	452.0	0.99			252.5
0039	6	×					4409929	6110	310	307.0		6.5	301.0	320.5	19.5	280.0	332.5	52.5	205.0	359.5	154.5
0136		×					4408355	6295	418	415.0	421.5	6.5	411.0	431.5	20.5	394.0	444.5	50.5	;		193.0
U013	- ·	×	221	18E	7 S	59795	4406500	5180	118	125.0	119.0	c.c	108.0	123.0	15.0	5.001	5 8 2 1	31.0	0.19	181.5	5.57 0.17
10015	7 5	< ×					4399709	2696	81	79.0	83.5	5.4	76.0	87.5	2.7	585	94.0	25.5	32.0	103.5	21.5
U003	3	: ×					4406488		513	510.5	518.5	8.0	507.5	526.5	19.0	504.0	550.5	46.5			114.5
U093	3	×		19E			4405761		575	572.5	578.0	5.5	569.5	588.0	18.5	564.0	612.0	48.0	516.0	634.0	118.0
000n	6	×					4400617	5887	520	518.5	521.0	2.5	516.0	524.5	8.5	510.0	534.0	24.0			59.0
U005		×	12S	19E	30 SI		4400542	5556	131	3 021	0.101	3.0	123.5	134.5	11.0	3.031	0.000	31.0	0 761	0.000	76.5
4304733243		×			4 4 N N	C 62248	4401302	5982	181	1173.5	1178.0	C. 4	0.//1	1178.5	10.5	0.7911	1205.0	38.0	135.0	240.0 1232.0	104.0
4304733185	< ×				22 SL		4401228	6463	1099	1095.5	1103.0	7.5	1090.5	1107.5	17.0	1089.0	1135.5	46.5	1050.5	1160.5	110.0
690N		×		21E		L 61993(	4400826	5496	130	129.5	133.0	3.5	125.0	134.5	9.5	123.0	150.5	27.5	86.5	172.5	0.98

APPENDIX continued

										Mahogany												
API US	USGS#	Type of Log	Twn	Rng	Sec	Mrd	UTME	UTM N	Elevation	Bed		50 GPT Zone			35 GPT Zone			25 GPT Zone		15 (	15 GPT Zone	
	Den	Fischer Son Assay							Ground level	Depth to bed	Top	Bottom	Thick- ness		p Bottom	Thick- n ness	Top	Bottom	Thick- ness	Top	Bottom	Thick- ness
UC	0070	×	12S	21E	35	ST	625945	4398702	5829	129	1 -		4.0	1 1			1 -		29.0	86.5	174.0	87.5
4304733131	< >		221		٠ 4	7 2	634037	4400902	4670 5826	714					-			_	46.0	649.0	769.0	120.0
4304733262	< ×		12S		30	SF	628635	4400487	6251	808			6.0		0 819.5			838.0	39.5	762.0	868.5	106.5
4304734730	×		12S	23E	Ξ	SF	645351	4405221	6004	700			_						63.5	579.5	746.0	166.5
4304733489			12S		16	SF	641989	4403238	5964	651									49.0	579.0	703.0	124.0
Ď	7800	×	12S		36	SL	646100	4398839	6362	465	461.0	469.5	8.5	458.0			432.5		63.0	303.0	500.0	197.0
Ö	410	×	12S			SF	656357	4406641	6340	306									53.5	;		150.0
	U055	×	12S		m t	S	653158	4407920	6137	465	462.0	468.0					442.0		49.5	320.5	498.0	177.5
4504/35083	X X X	,	271	24E	- 5	7 5	655201	4404973	0000	380			0.0						5.55	2,60	0.250	5.001
0 1	130	×	271		7 7	7 2	102550	4402783	0110	C/			0.7						C: /4	0.07	C./+I	5.121
5	U091	×	271	24E 24E	<u> </u>	7 2	654533	4403991	6300	385		380.5		377.5		26.0		88.0	48.5 37.5	0.0	133.3	135.3
	C+10	< >	12.5		01	2 2	648046	4402078	1909	504	499.0		_				470.0		2.75	318.0	547.5	220 5
5 5	1134	< >	12.5		3 2	2 2	652365	4402076	6225	140			11.0		5 601				0.27	0.010		0 000
5	U153	< ×	128		3 %	2 2	656186	4401431	0999	100									46.5	25.0	170.5	145.5
) E	11141	: ×	12.8		75	5	196259	4399513	6450	100				0.00	117.5				0 09			196 5
Ď	0600	: ×	12S		36	S	626719	4399338	0069	73								102.0	58.0	0.0	183.5	183.5
in	U135	×	12S		7	SL	658311	4406094	6540	303	(*,	3		7	(*,				51.0			161.5
in	U143	×	12S		17	SL	658938	4403501	00/9	192							169.5		45.5	141.5	284.5	143.0
ñ	U152	×	12S	25E	17	SL	658452	4404632	0099	212	209.0			(4					40.5	184.0	287.5	103.5
Ü	U140	×	12S	25E	18	SL	657356	4403625	6340	91									54.5	15.0	173.5	158.5
ŭ	U017	×	13S	18E	4	SL	594250	4396676	0609	129		131.0	3.5				117.0		25.5			66.5
ŭ	U018	×	138		7	$_{ m ST}$	299386	4394268	6275	115			3.5		0 119.0				19.5			51.0
ŭ	0008	×	138		4	$_{ m ST}$	605853	4393568	6247	167	162.5	167.5	5.0	162.0					26.0			0.89
) O	U010	×	138		34	ST	604747	4388476	6763	158									5.0	148.0	172.5	24.5
Ď	U023	×	138			ST	618235	4396672	5836	167	164.0	168.5		157.5			155.5	184.0	28.5	152.0	226.5	74.5
Ď;	U021	×	138		∞ :	SF	610525	4396747	5964	167	164.5	_							25.0	148.0	214.0	66.4
Ö	U159	×	138		= ;	SL	616915	4395010	5908	92.									25.0	33.0	105.5	72.5
ĭ :	U022	×	138		4 %	S	615775	4394255	6038	158	156.5			_					22.5	142.5	203.5	61.0
o F	0100	×	135		97 5	Z 5	21/219	4389681	6588	8 6	7.8/								18.0	04.0	106.0	42.0
Ċ	0161	×	25.		15	Z 5	618866	43889/3	645/	0/		5.0/		0.00					16.5	32.0	5.06	38.5
5 2	00/9	×	135	22E	5 5	75	633812	1,656,64	7750	460			3.0						0.72	5.77	1545	5.201
	11074	< >	13.0		3 1	2 2	746670	4380740	8678	148									24.0	102.5	180.0	3.5
	1072	< ×	138		35	S	635700	4389409	0029	120			5.0						33.5	43.0	146.0	103.0
ñ	U073	: ×	138		35	SL	635749	4388635	6727	53	51.5	56.5							30.5	15.0	102.5	87.5
ŭ	9200	×	13S	23E	56	SL	644861	4390642	6419	33									42.0	0.0	120.5	120.5
U	U027	×	13S	24E	7	SL	654287	4397281	6829	121	116.0								56.5	0.0	179.5	179.5
Ü	U177	×	138	24E	7	$S\Gamma$	654056	4398315	6611	49									53.5	0.0	170.0	170.0
ď	U077	×	138		9	ST	648138	4397625	6268	190		194.0				0 25.5			62.5	35.0	238.0	203.0
Ď	U041	×	138		∞	SL	649145	4395648	6322	89									45.5	0.6	153.5	144.5
กั	U042	×	138		6	SL	651527	4396110	6497	66	0.86	,	6.5						45.0	0.0	148.5	148.5
Ď	U078	×	138		10	SF	652681	4395938	229	159		163.5							61.0	0.0	204.5	204.5
ă È	0094	×	24.		8 2	Z 5	619333	4384393	09/9	81									0.11	71.0	57.5	21.5
51	0.093	×	24. 2.4.	21E	70	7 2	625617	120864	700/	00	62.0	0.4.0	1.0						9.0	0.4.0	C. 4.0	2.02
5 5	0017	< ×	158		<u>†</u> 2	3 2	626861	4376431	7187	77									1.5	70.0	82.5	12.5
ŭ	960 N	×	158		17	SF	621043	4374385	7282	107	106.0	107.5	1.5	104.0	0 108.5		103.0	112.0	9.0	0.86	115.5	17.5
ŭ	860N	×	15S		34	$_{ m ST}$	633492	4369213	7542	54			5.0	54.		0.2.0	53.0		4.0	50.0	58.0	8.0
U	660	×	16S	22E	23	$S\Gamma$	633476	4361817	7728	40			0.0	39.		0 1.0	37.0		3.5	36.0	44.0	8.0
N	Lan collect																					

Note: Numbers in italics indicate estimates

Den = Bulk density log, Son = Sonic log, Twn = Township, Rng = Range, Sec = Section, Mrd = Meridan, SL = Salt Lake Base Line and Meridian, UN = Uinta Special Meridian, GPT = gallons shale oil per ton of rock